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# Ultra-High Temperature Mechanical Properties of Zirconium Diboride-Based Ceramics

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# **Ultra-High Temperature Mechanical Properties of $ZrB_2$ -Based Ceramics**

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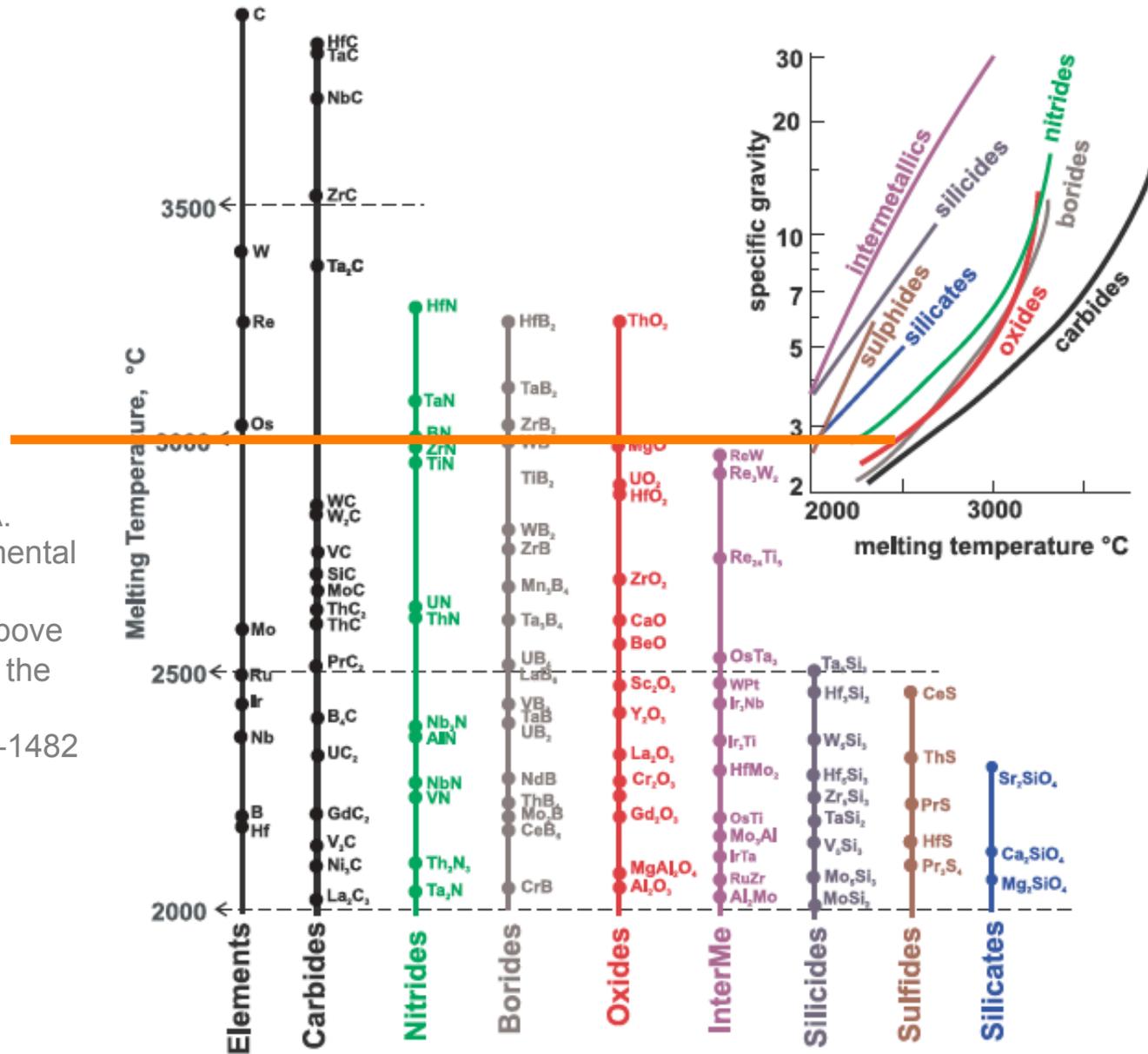


# Acknowledgement

- **Dr. Eric Neuman**
  - **Dissertation research**
- **Drs. Jeremy Watts, Harlan Brown-Shaklee, and Eric Neuman**
  - **Building UHT mechanical testing system**
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# High Melting Temperature Materials

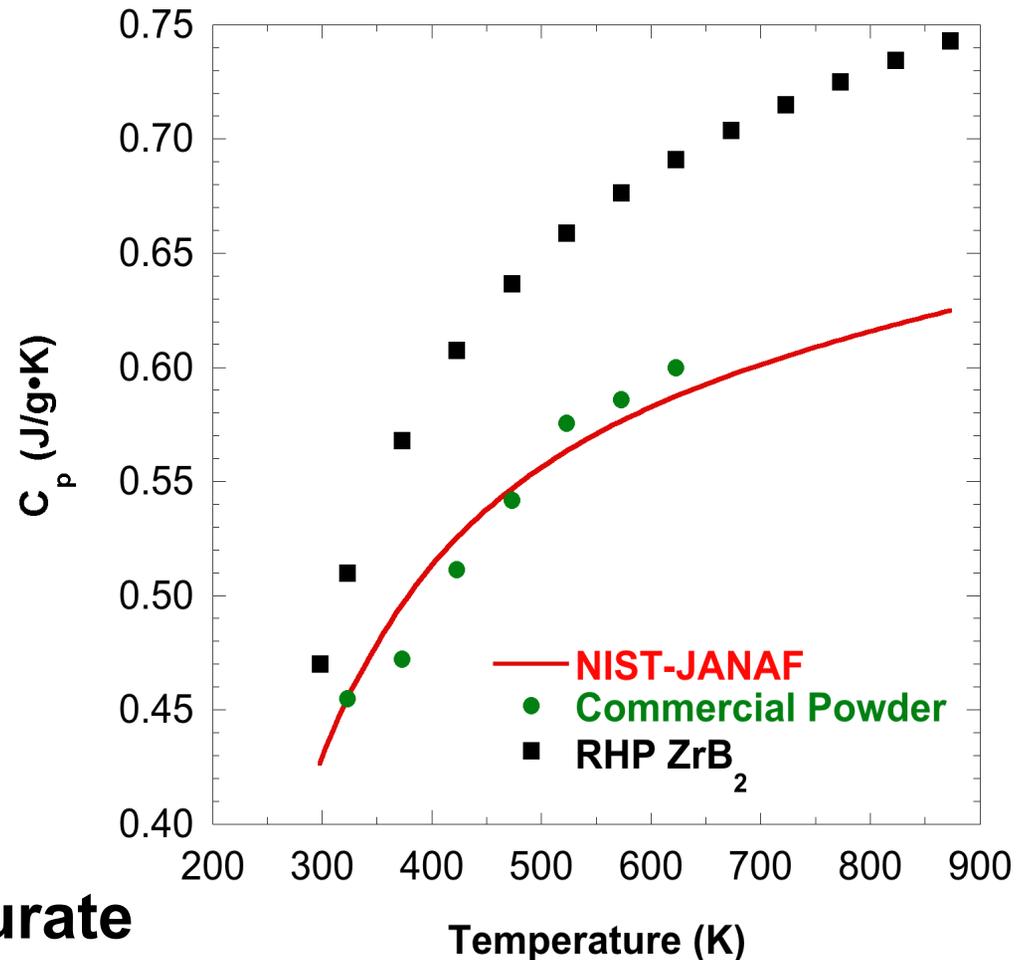


S.V. Ushakov and A. Navrotsky, "Experimental Approaches to Thermodynamics above 1500°C," Journal of the American Ceramic Society, 95(5) 1463-1482 (2012).



# Motivation and Purpose

- Intrinsic properties
  - Measuring is simple conceptually, but difficult in practice
- Thermal conductivity
  - Impurity effects
  - Lack of single crystals
- Heat capacity
  - Historic data are inaccurate

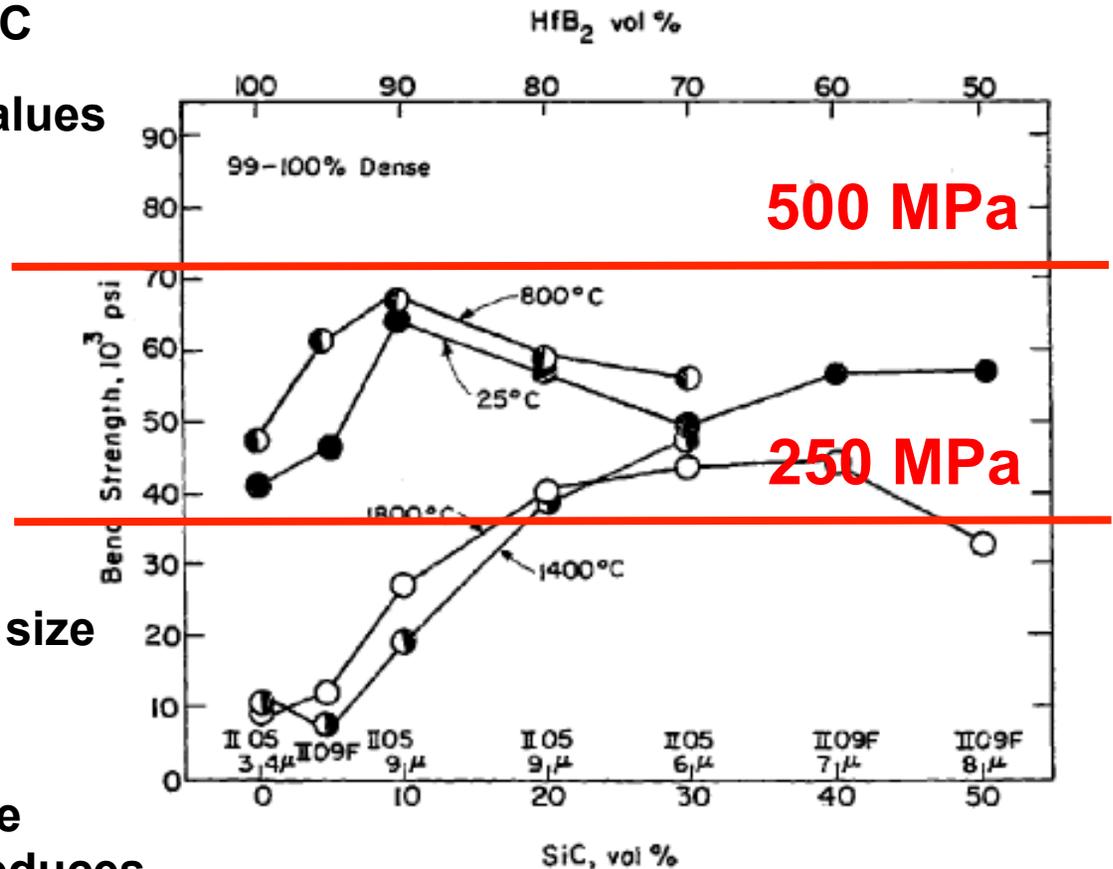


**Systematically study the mechanical behavior of  $ZrB_2$ -based ceramics at ultra-high temperatures**



# Historic Strength Studies

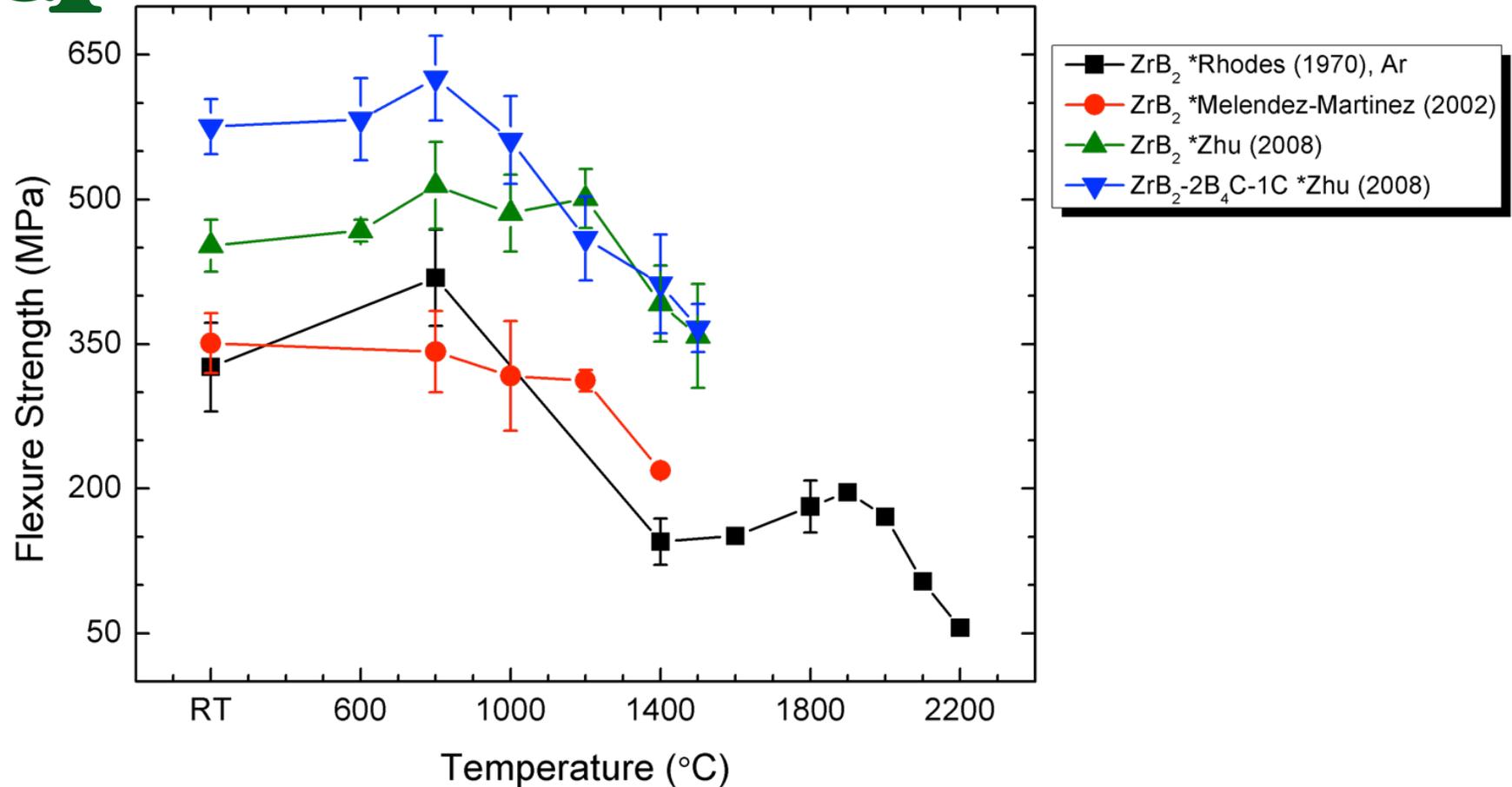
- Strength tested up to 2200°C
- Range of relative density values
- ZrB<sub>2</sub> and HfB<sub>2</sub>
  - Nominally pure
  - SiC additions
  - Carbon additions
- Porosity reduces strength despite a decrease in grain size
- SiC reduces grain growth
- Carbon improves resistance to crack propagation and reduces elastic modulus



50 ksi ≈ 350 MPa



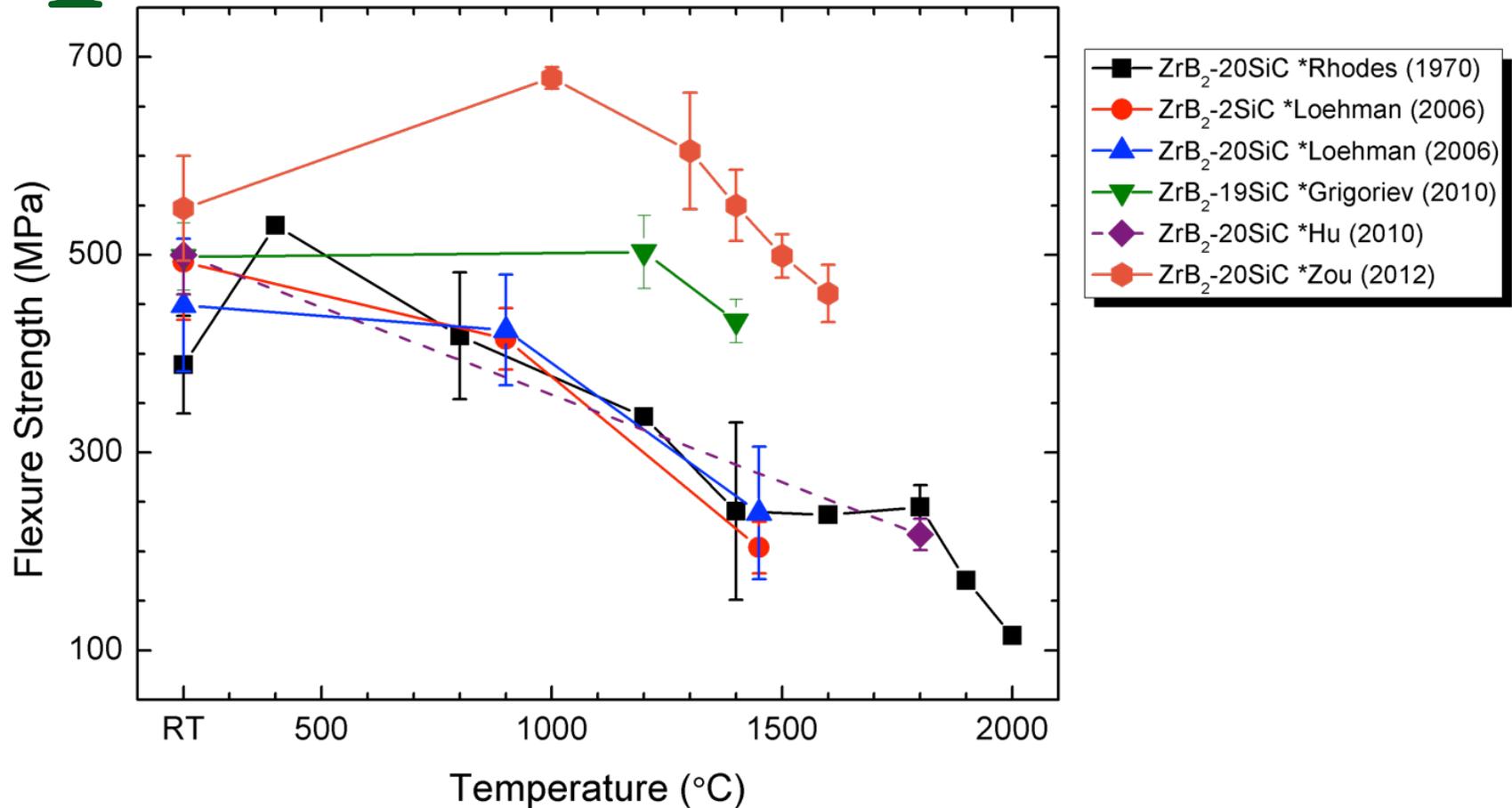
# ZrB<sub>2</sub> Strength vs. Temperature



- Limited studies of ZrB<sub>2</sub> at elevated temperatures
- ZrB<sub>2</sub> strength decreases as grain size increases
- Diffusional creep limits strength at the highest temps



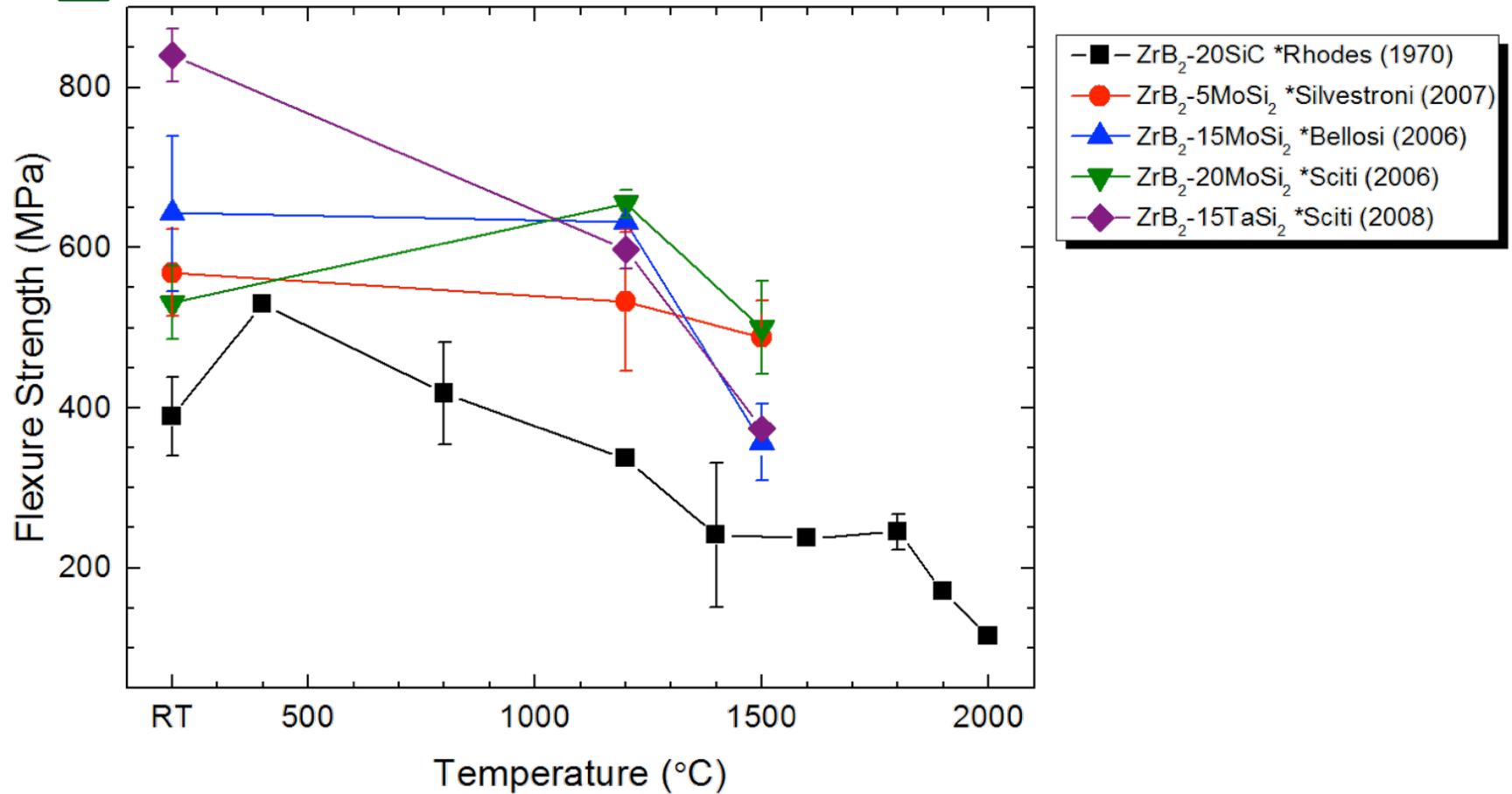
# ZrB<sub>2</sub>-SiC vs. Temperature



- More studies than pure ZrB<sub>2</sub>, but few over 1600°C
- ZrB<sub>2</sub>-SiC eutectic at 2270°C limits upper use temperature



# ZrB<sub>2</sub>-Disilicide vs Temperature

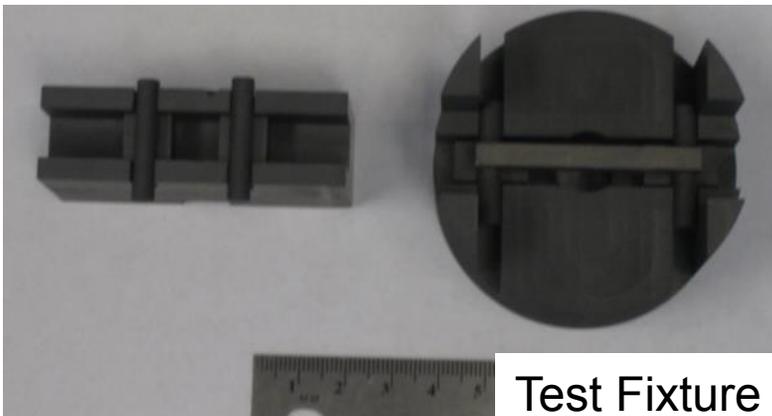


- Disilicide additions can improve strength compared to SiC
- No studies of ZrB<sub>2</sub> with silicides above 1500°C
- Use limited by T<sub>melt</sub> (MoSi<sub>2</sub> - 2030°C; TaSi<sub>2</sub>- ~2200°C)



# UHT Mechanical Test System

- Instron 33R4204 load frame
- Custom-built environmental chamber
  - Inert atm or mild vacuum
  - $\sim 10^{-14}$  atm pO<sub>2</sub> using Ar
- Induction heating system
  - Capable of 2600°C
  - Heating rate of 100's°C/min
- Graphite load train and test fixture
- Testing limited by phase stability
  - Ex: ZrB<sub>2</sub>-C eutectic at 2370°C



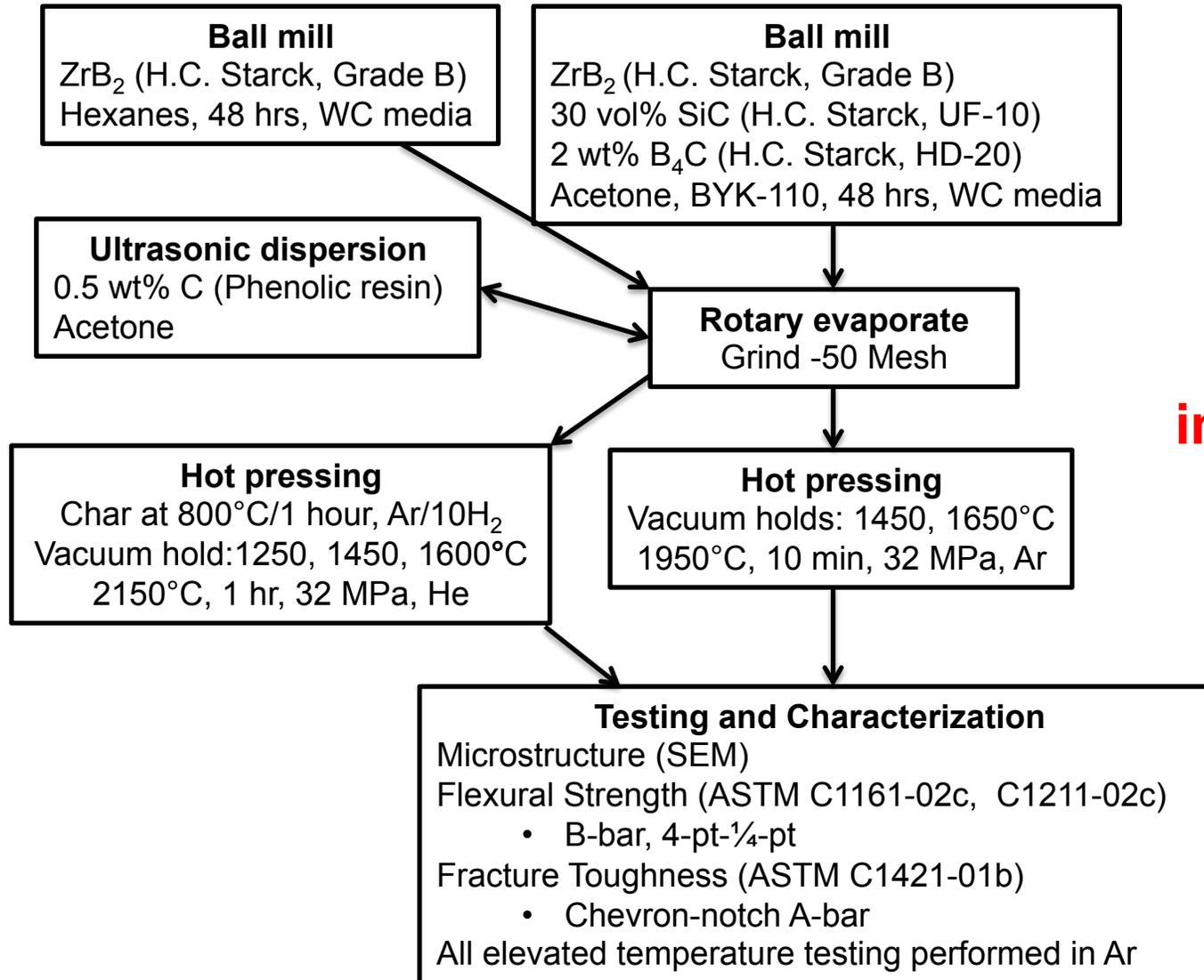
Test Fixture



# Processing

## ZrB<sub>2</sub>

## ZrB<sub>2</sub>-30SiC

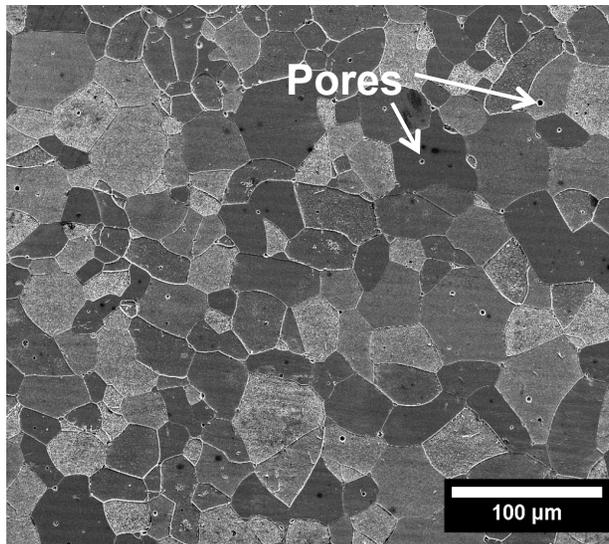


**Room for improvement?**



# Microstructures

**ZrB<sub>2</sub>**



**99.2% dense**

**Grain size: 19.7 ± 13.0 μm**

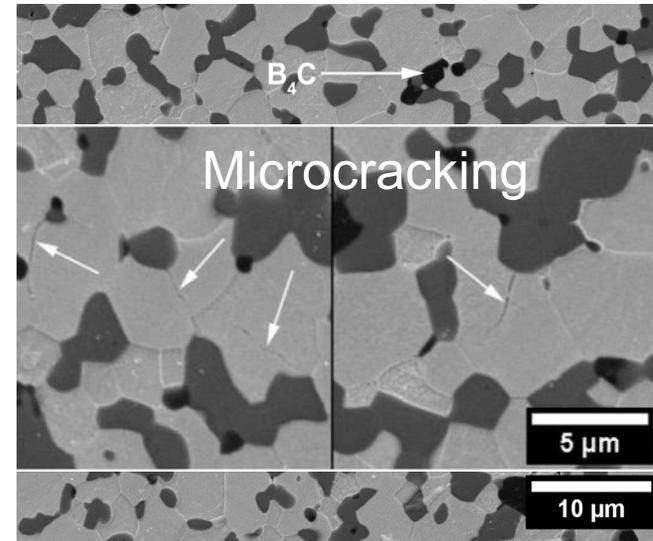
**Held at 2150°C for 1 hr**

- **Grow grains and reduce creep above 1800°C**

**Minimal entrapped porosity**

**No residual carbon**

**ZrB<sub>2</sub>-30SiC**



**>99.9% dense**

**ZrB<sub>2</sub> grain size: 1.9 ± 0.9 μm**

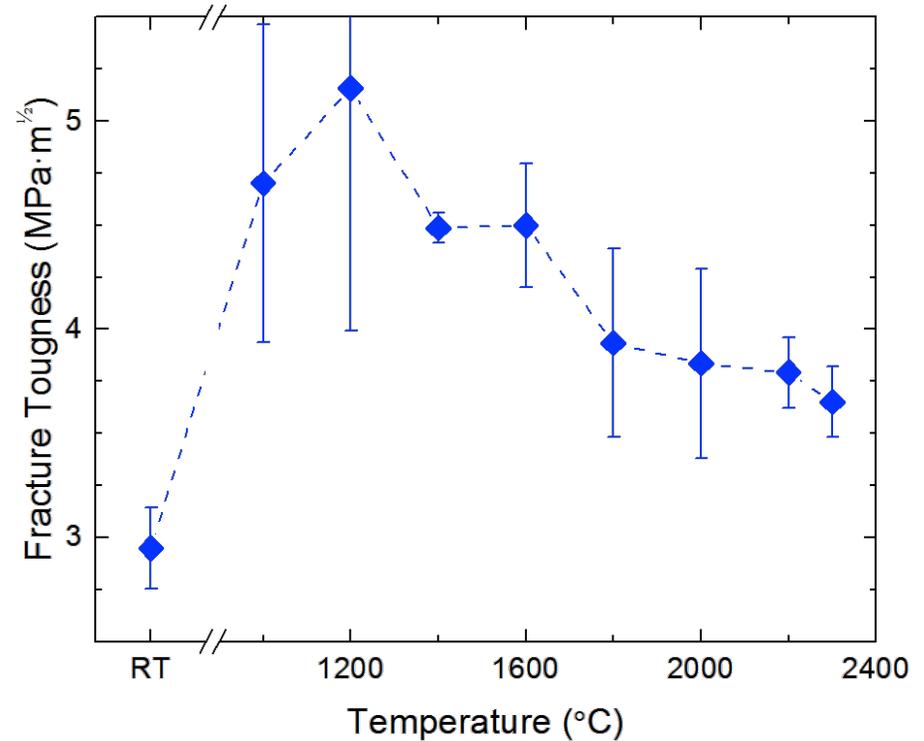
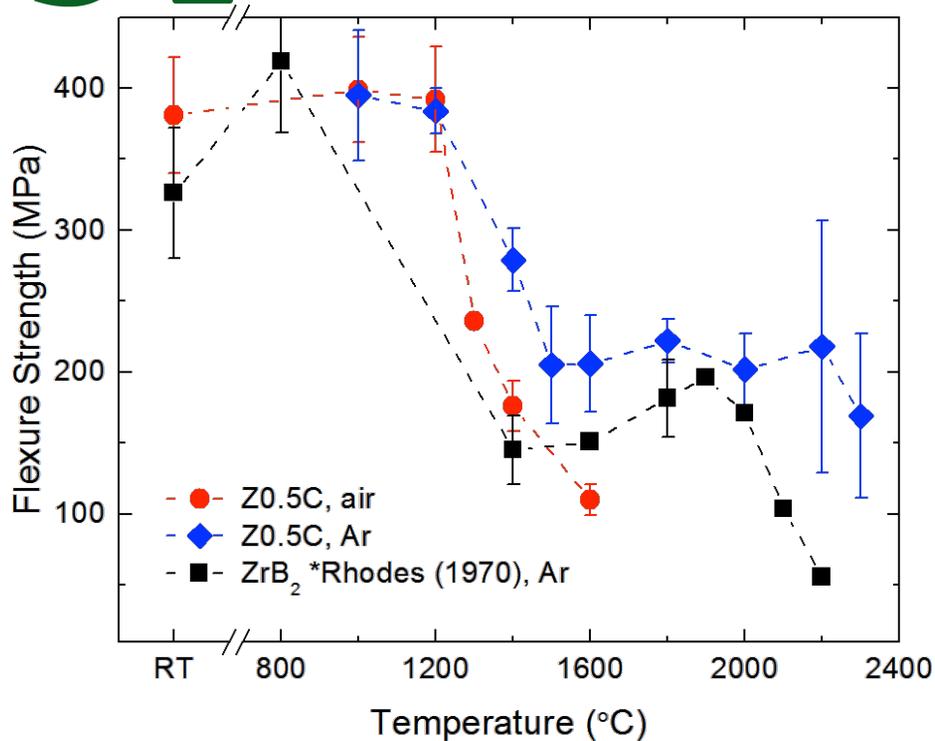
**SiC cluster size: 6.1 ± 4.4 μm**

**Max SiC cluster size: 59.1 μm**

**Micracking threshold ~ 15 μm**



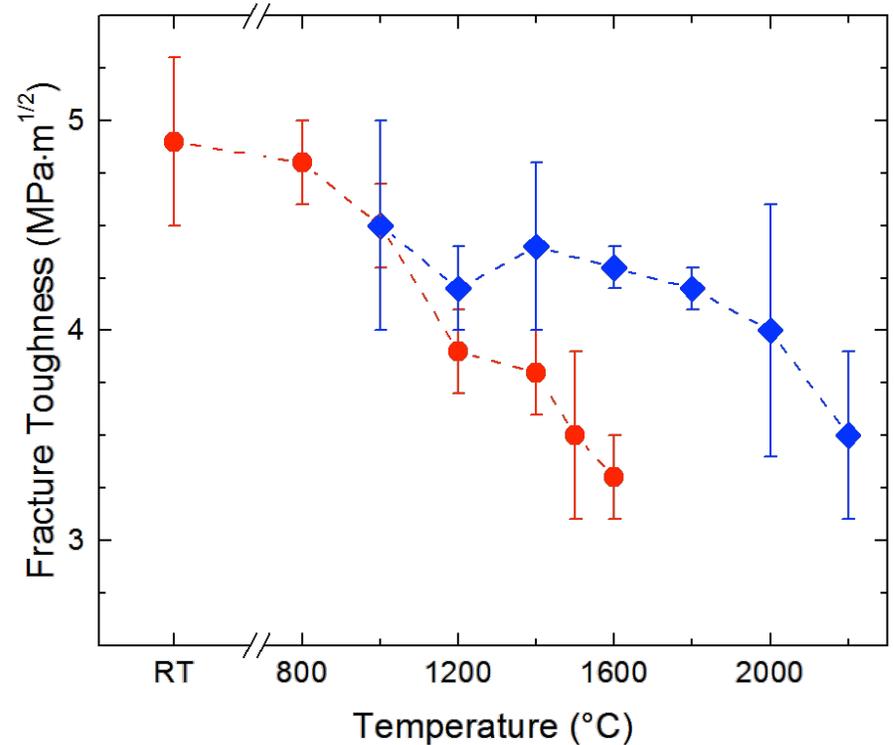
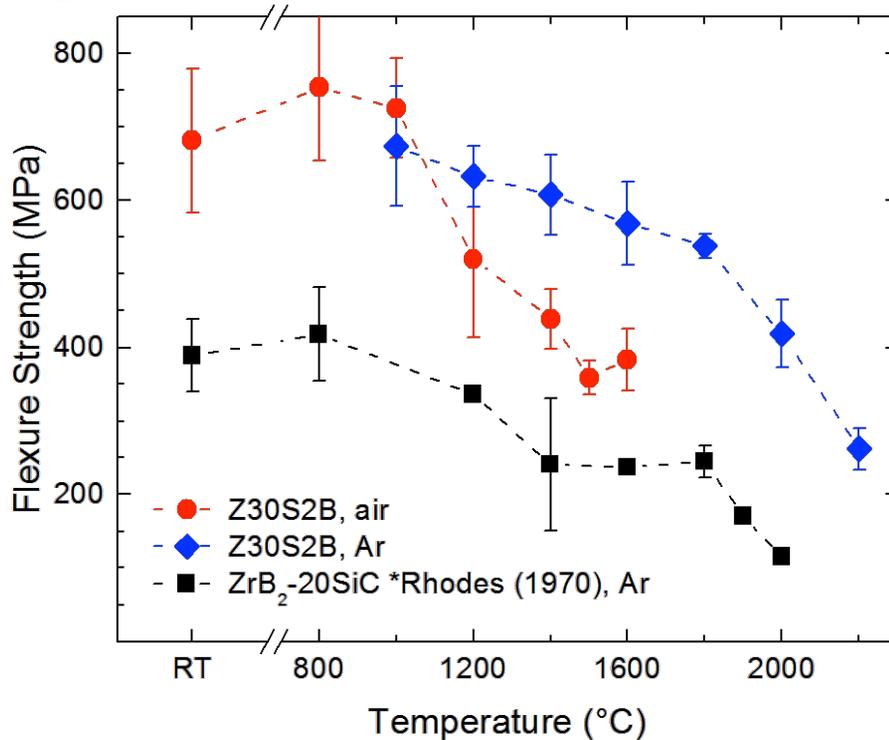
# ZrB<sub>2</sub> Strength and Toughness



- **Air: Strength 300-400 MPa up to 1200°C, ~200 MPa above (oxidation)**
- **Inert: Strength stabilizes at ~200 MPa up to 2300°C (creep?)**
- **Critical flaw size consistent with grain size at elevated temperatures**
  - **Grain growth during tests at 2000°C and above**



# ZrB<sub>2</sub>-SiC Strength and Toughness



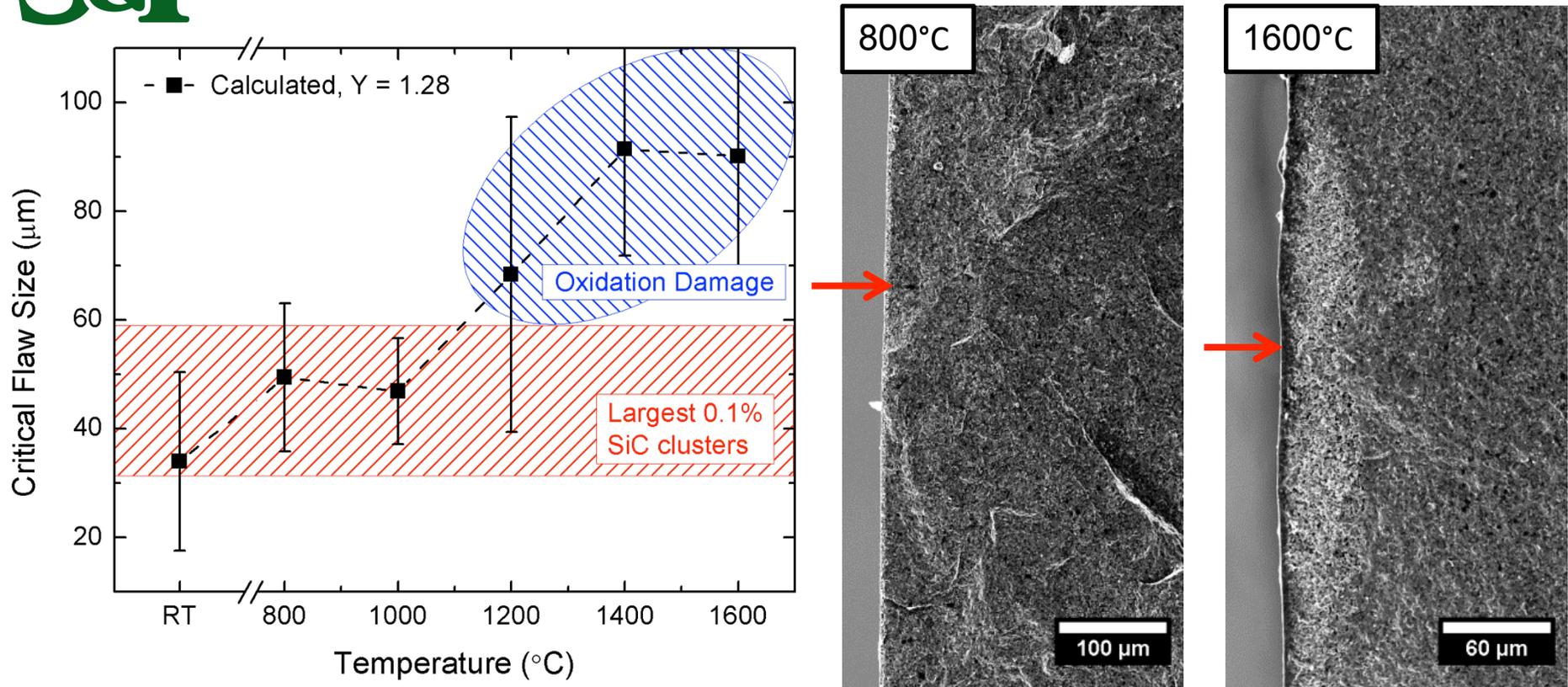
- **Air:**  $\sigma$  increases  $\leq 1000^\circ\text{C}$  (flaw healing), decreases  $> 1200^\circ\text{C}$  (oxidation)
- **Inert:**  $\sigma > 550$  MPa up to  $1800^\circ\text{C}$ , decreases to 2200 MPa at  $2200^\circ\text{C}$
- **Both:**  $K_{IC}$  decreases steadily from  $\sim 4$  MPa·m<sup>1/2</sup> at RT to  $\sim 3.5$  MPa·m<sup>1/2</sup>

Neuman, et al., *J. Euro. Ceram. Soc.*, 33[15-16] 2889-2899 (2013)

Neuman, et al., *J. Euro. Ceram. Soc.*, 35[2] 463-476 (2014)



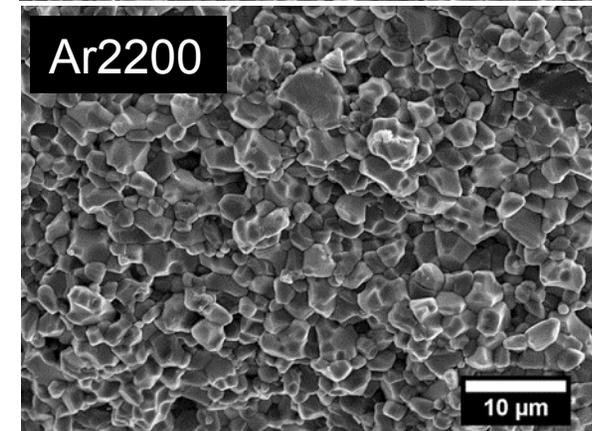
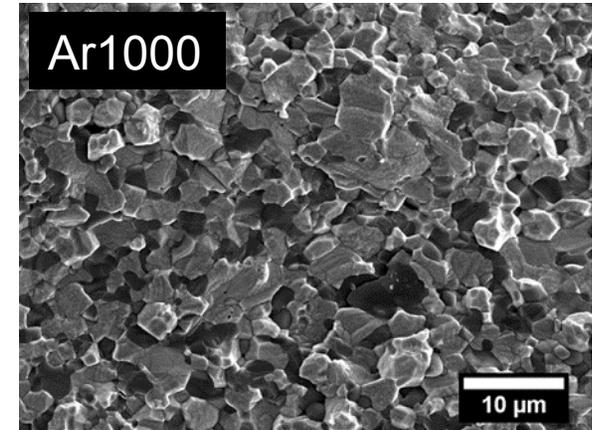
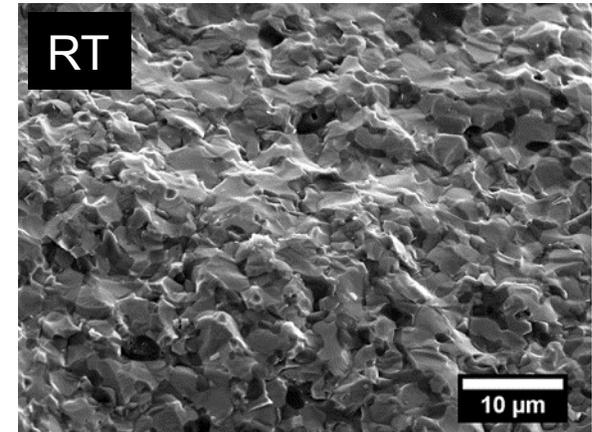
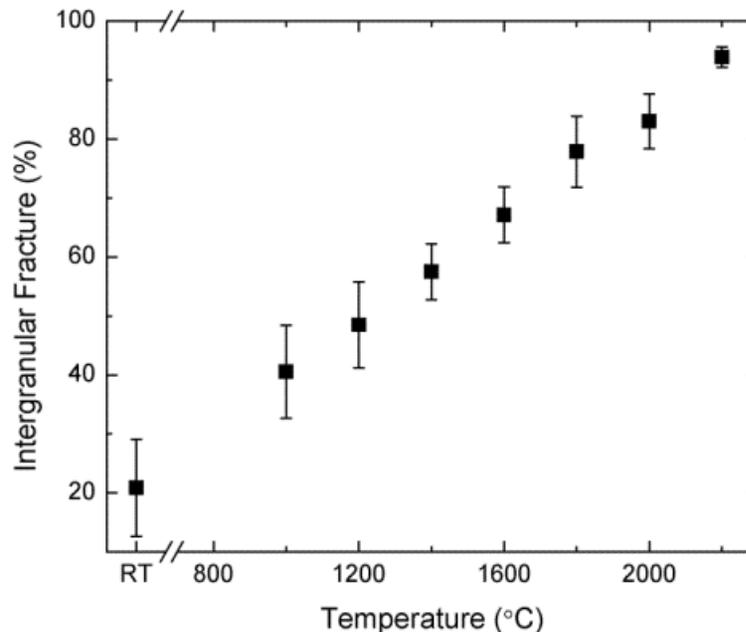
# ZrB<sub>2</sub>-SiC Failure Analysis



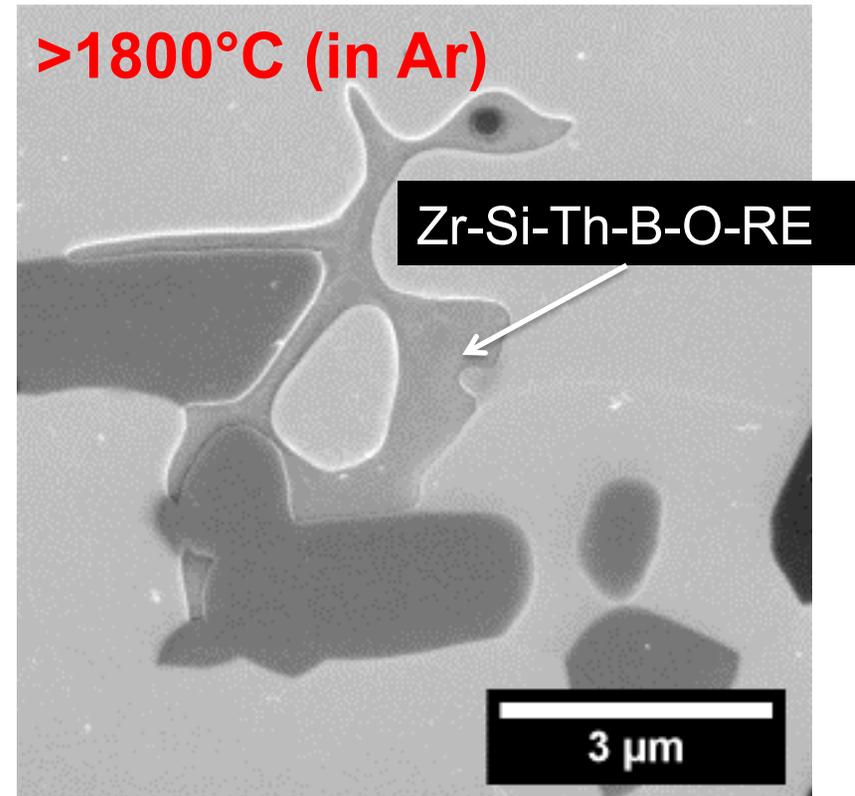
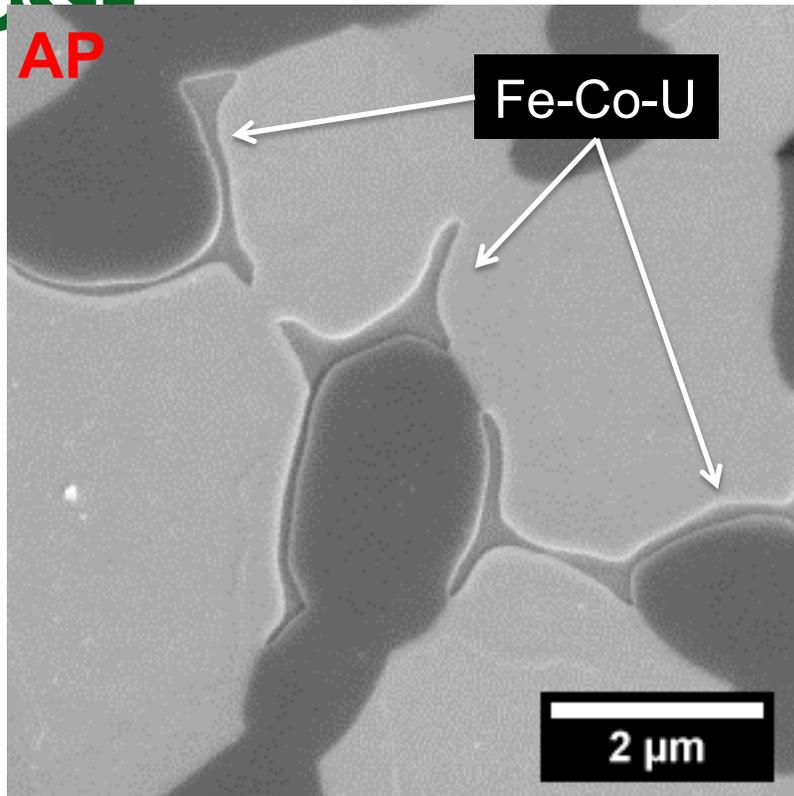
- **Below 1000°C, SiC clusters are the critical flaw**
- **Oxidation damage controls strength at ≥1200°C (3 pt. bending of bar halves)**
- **Observed fracture origins are consistent with size of calculated critical flaws**
- **Improve strength by reducing SiC cluster size or reducing oxidation damage**

# ZrB<sub>2</sub>-SiC Fracture in Argon

- ~20% intergranular fracture at RT
- Fraction steadily increases with temperature
  - Trend contrary to historic reports
  - SiC cluster size grows >1800°C
- **Lower temp. tests do not predict UHT strength**



# Oxide Impurity Phases



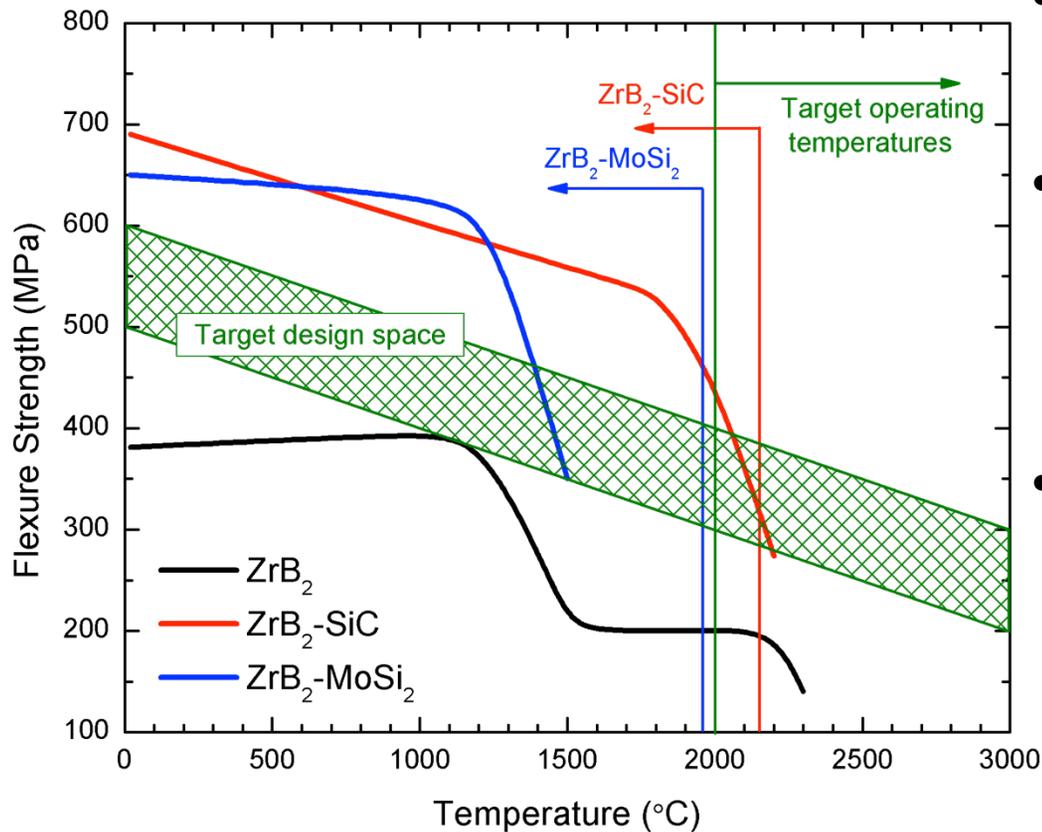
- Fe, Co, U containing phase present following hot pressing
  - Appears wetting to both  $ZrB_2$  and SiC
  - Possibly a silicide phase – Reduction of SiC by Fe and Co



# Can We Increase Use Temperature?

What are we looking for?

- **Chemical stability at 2000°C+**
- **Second phase additions**
  - Improve properties
  - Enhance densification
- **Higher eutectic temps**
  - ZrB<sub>2</sub> – SiC at 2270°C
  - ZrB<sub>2</sub> – ZrC at 2660°C
  - ZrB<sub>2</sub> – ZrC<sub>0.88</sub> at 2830°C
  - HfB<sub>2</sub> – HfC<sub>0.9</sub> at 3140°C



# Processing

## ZrB<sub>2</sub>

### Ball mill

ZrB<sub>2</sub> (H.C. Starck, Grade B)  
Hexanes, 48 hrs, WC media

## ZrB<sub>2</sub>-30SiC

### Ball mill

ZrB<sub>2</sub> (H.C. Starck, Grade B)  
30 vol% SiC (H.C. Starck, UF-10)  
2 wt% B<sub>4</sub>C (H.C. Starck, HD-20)  
Acetone, BYK-110, 48 hrs, WC media

## ZrB<sub>2</sub>-10ZrC

### Ball mill

ZrB<sub>2</sub> (H.C. Starck, Grade B)  
9.5 vol% ZrC (H.C. Starck, B)  
0.1 wt% C (Phenolic resin)  
1.2 mol% ZrH<sub>2</sub> (Chemetall, S)  
MEK, BYK-110, 24 hrs, ZrB<sub>2</sub> media

### Ultrasonic dispersion

0.5 wt% C (Phenolic resin)  
Acetone

### Rotary evaporate

Grind -50 Mesh

### Hot pressing

Char at 800°C/1 hour, Ar/10H<sub>2</sub>  
Vacuum hold: 1250, 1450, 1600°C  
2150°C, 1 hr, 32 MPa, He

### Hot pressing

Vacuum holds: 1450, 1650°C  
1950°C, 10 min, 32 MPa, Ar

### Hot pressing

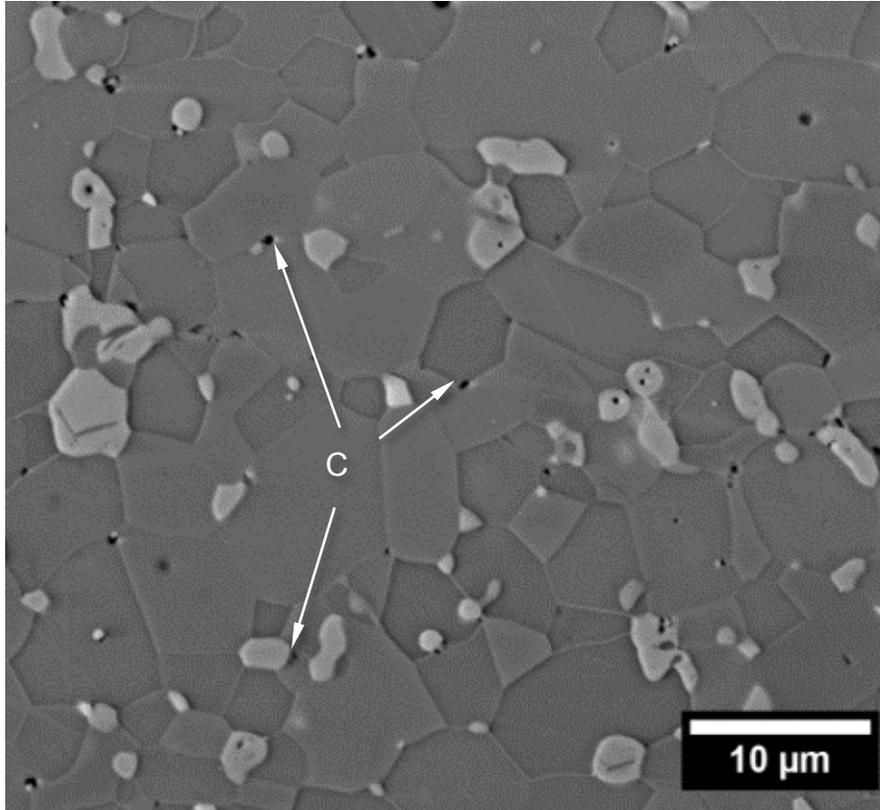
Char at 800°C/1 hour, Ar/10H<sub>2</sub>  
Vacuum hold: 1250, 1450, 1600°C  
1900°C, 45 min, 32 MPa, Ar/10H<sub>2</sub>

### Testing and Characterization

Microstructure (SEM)  
Flexural Strength (ASTM C1161-02c, C1211-02c)  
• B-bar, 4-pt-¼-pt  
Fracture Toughness (ASTM C1421-01b)  
• Chevron-notch A-bar  
All elevated temperature testing performed in Ar



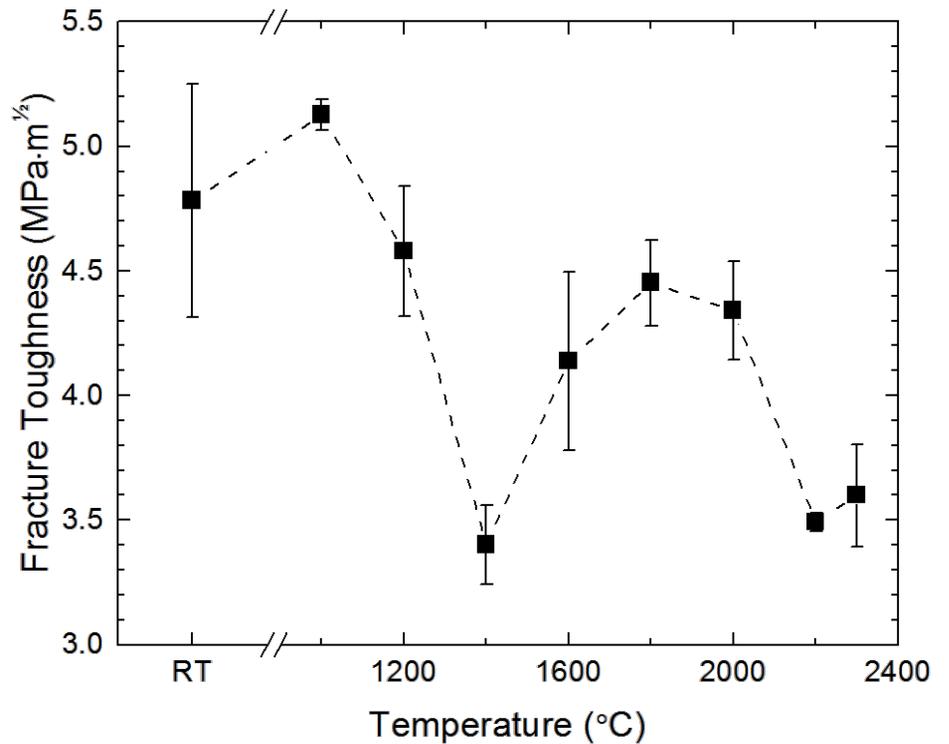
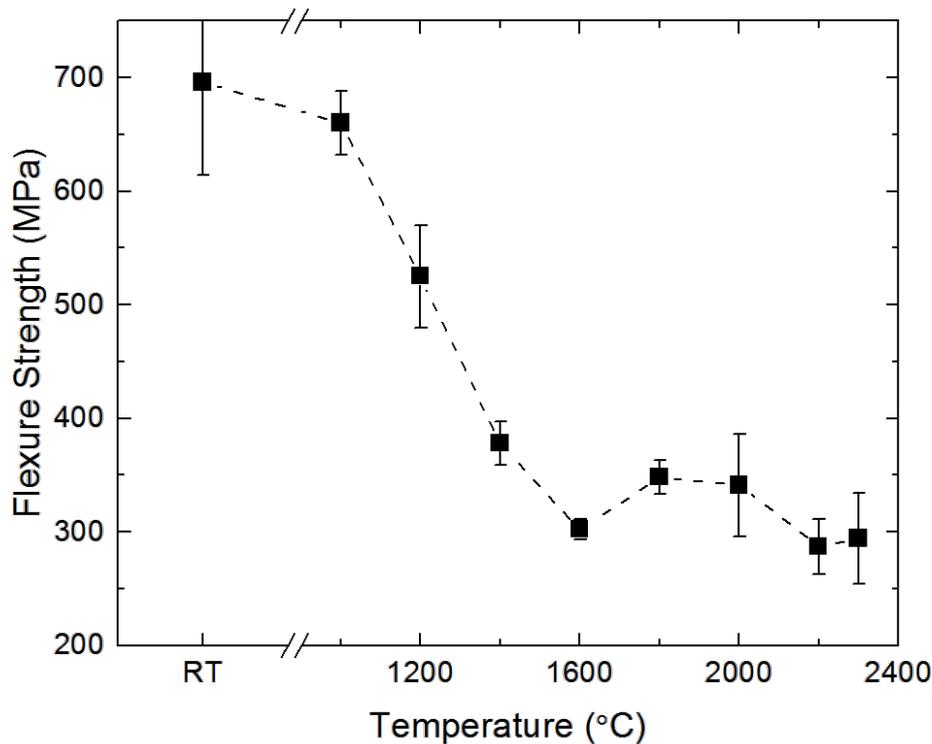
# ZrB<sub>2</sub>-10ZrC Microstructure



- >99% dense
- ZrB<sub>2</sub> grain size  $4.9 \pm 3.0 \mu\text{m}$
- ZrC cluster size  $1.8 \pm 1.5 \mu\text{m}$
- Max ZrC cluster  $9.8 \mu\text{m}$
- $9.5 \pm 0.4 \text{ vol\% ZrC}$
- $0.10 \pm 0.02 \text{ vol\% C}$
- $0.05 \pm 0.02 \text{ vol\% porosity}$

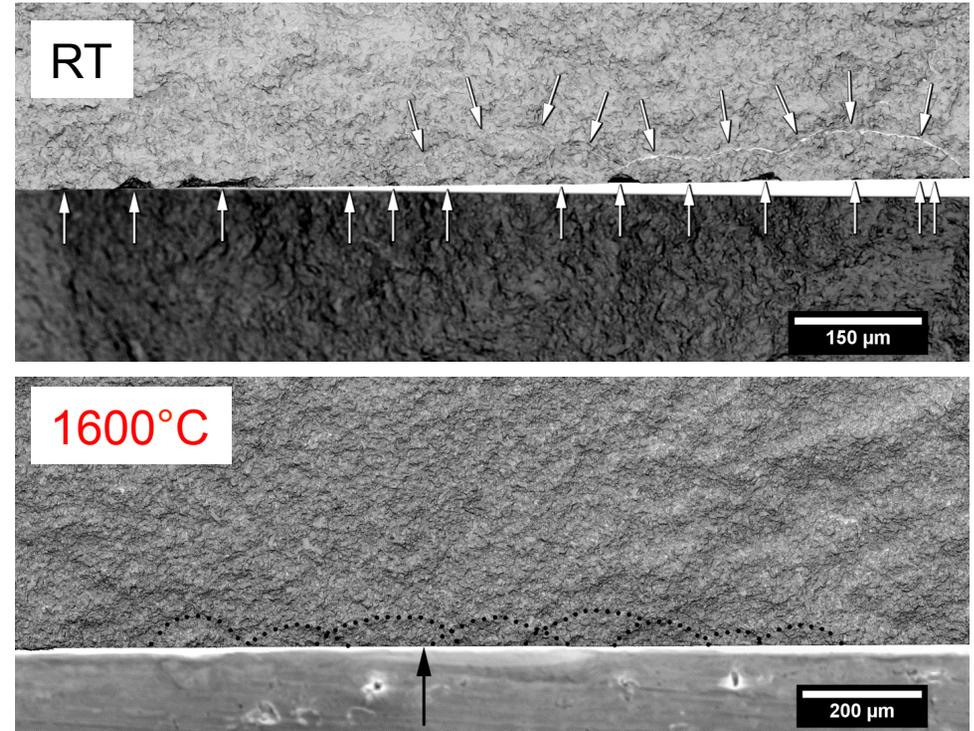
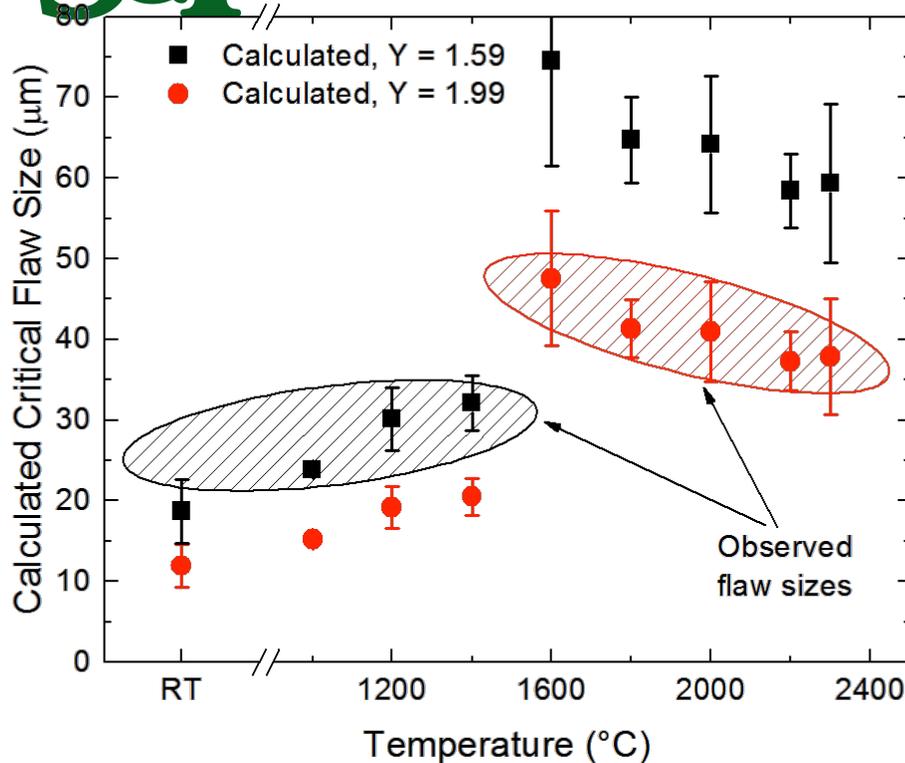


# ZrB<sub>2</sub>-ZrC Strength and Toughness



- **Strength decreases from ~700 MPa at 800°C to ~300 MPa at 1600°C**
  - **Maintains ~300 MPa up to 2300°C**
- **~4.5 MPa·m<sup>1/2</sup> at RT with no discernible trend**
  - **Minimum about temperature for relaxation of residual stresses**

# ZrB<sub>2</sub>-ZrC Failure Analysis



- Two regimes of failure behavior
  - 1400°C and below strength limited by machining damage
  - 1600°C and above controlled by subcritical crack growth
- Both related to original flaw population induced by machining



# Can We Get Higher Strengths?

- **Materials**

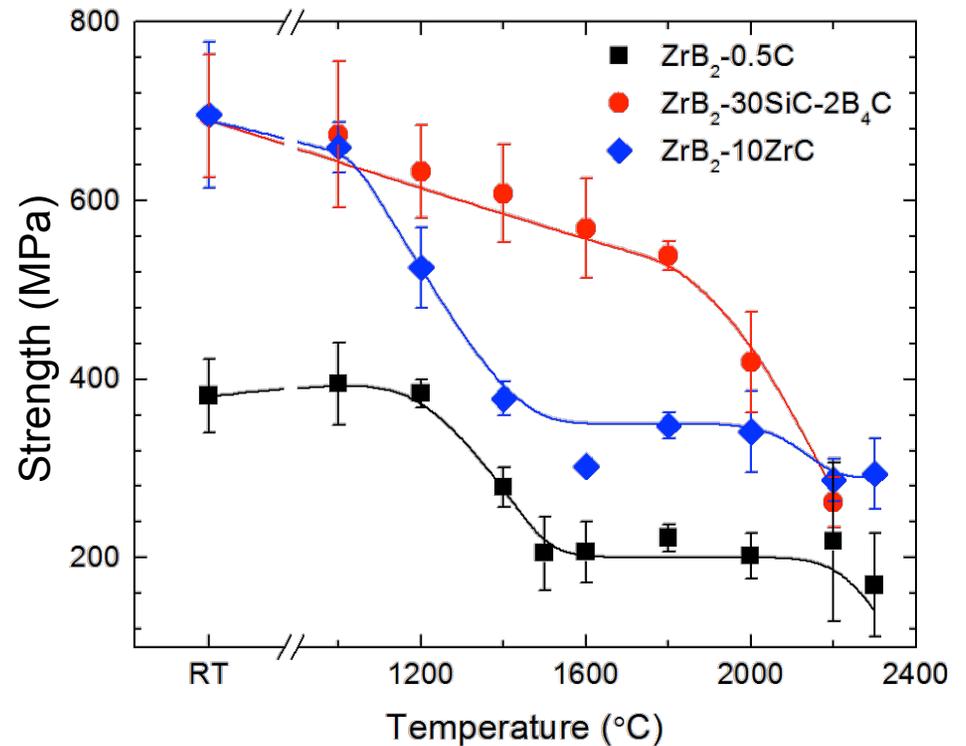
- Higher eutectic temperatures
- $\text{HfB}_2\text{-HfC}$ ,  $(\text{Hf,Ta})\text{C}$ , others?

- **Microstructures**

- Fully dense, no microcracks
- Grain size?? (creep vs  $\sigma$ )
- No grain growth at UHT??

- **Impurities**

- Eliminate undesired impurities (transition metals, oxides, etc.)
- Effects of doping or pinning??



**We have only scratched the surface for UHT structure-property relationship studies**

