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SiC-SiC CMCs Using BN powder coated silicon carbide fibers

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SiC – SiC CMCs using BN powder coated silicon carbide fibers

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C. Lewinsohn

November 8, 2017

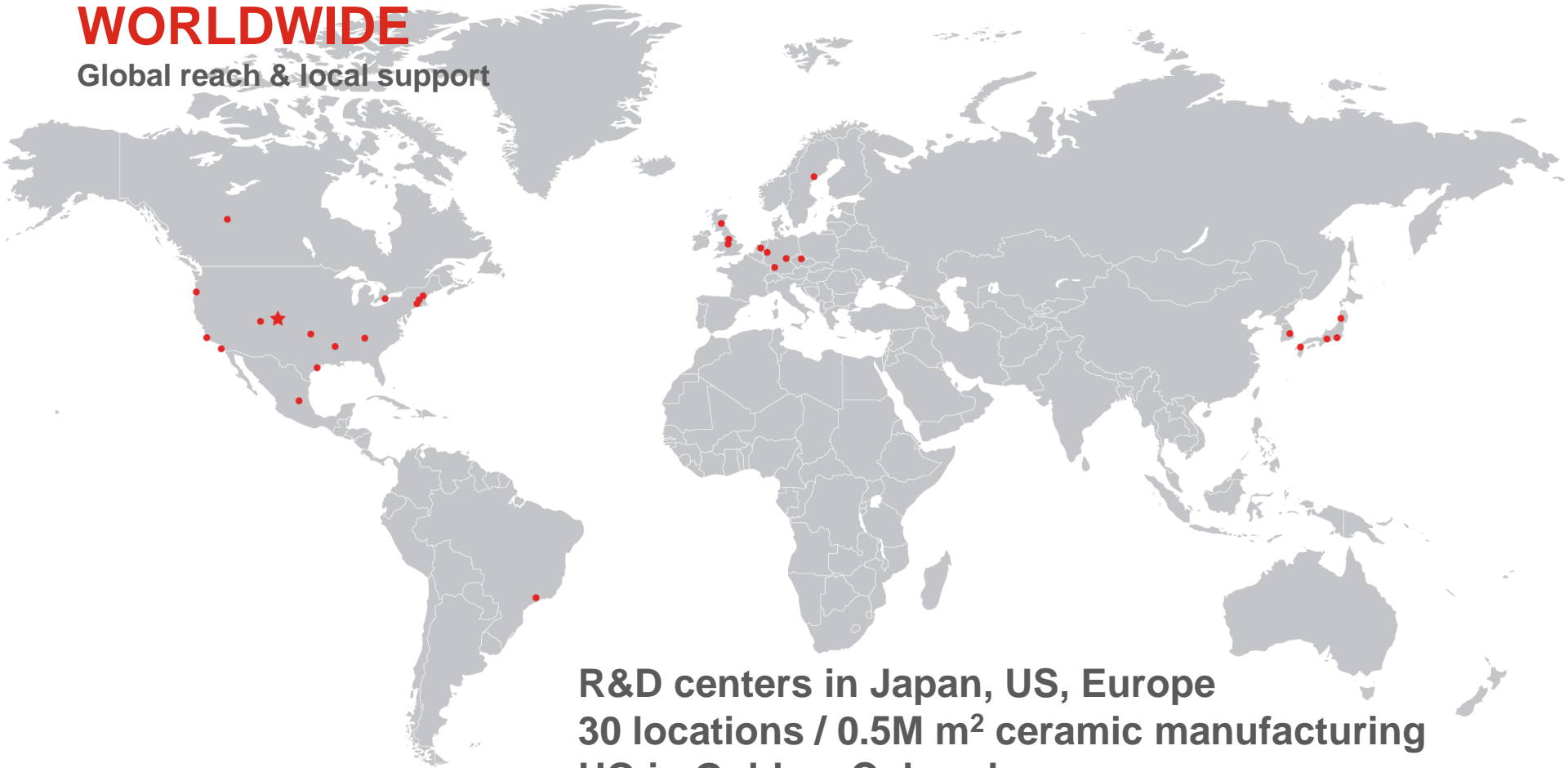
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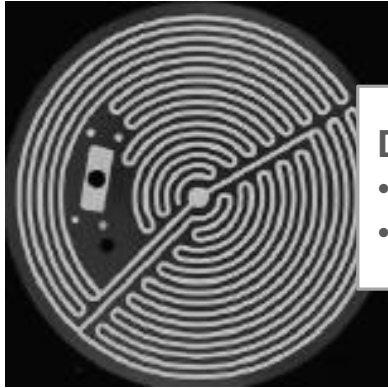
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Global reach & local support



R&D centers in Japan, US, Europe
30 locations / 0.5M m² ceramic manufacturing
HQ in Golden, Colorado

Silicon Carbide Processing at CoorsTek K.K.



Direct Sintered SiC

- CMP Plates
- Stage platforms

Reaction Bonded SiC

- Wafer boats
- Radiant tubes



SiC CMC

CVD SiC

- Process rings
- Showerheads



Carbon Fiber CMC

- Disc brakes
- Roller hearth



BN Powder Motivation

1. Performance

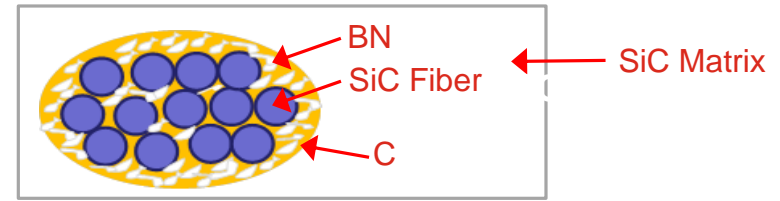
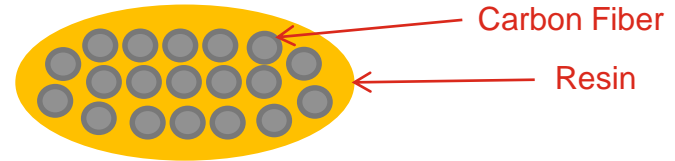
- Lessons from C-SiC composite experience
- Resin/slurry penetrates fiber bundles > BN slurry should be able to do the same

2. Process

- Melt Infiltration (MI) production
- Available BN powder & SiC fiber options
 - Denka, Showa Denko, Maruka
 - Ube Tyranno SA fiber (coat tows woven into fabric)

3. Value

- CVD alternative
- Lower cost / less hazardous



Mechanical Evaluation | SENB

Samples from ~ 16 layer composite

- ~45 mm x 15 mm x 5 mm
- 2 test bars per sample

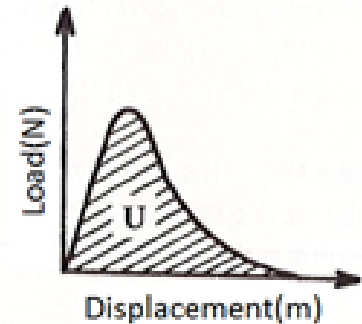
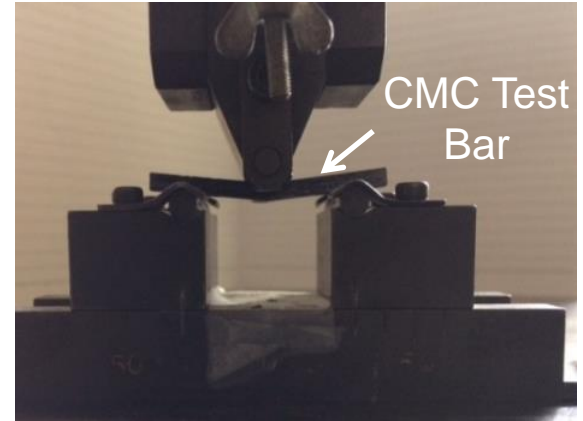
JCRS 201

- 40 mm L x 3 mm W x 4 mm D (ideal)
- Notch depth is half the height: typically 2mm
- 3-point flexure (30 mm span)
- 0.01 mm/min

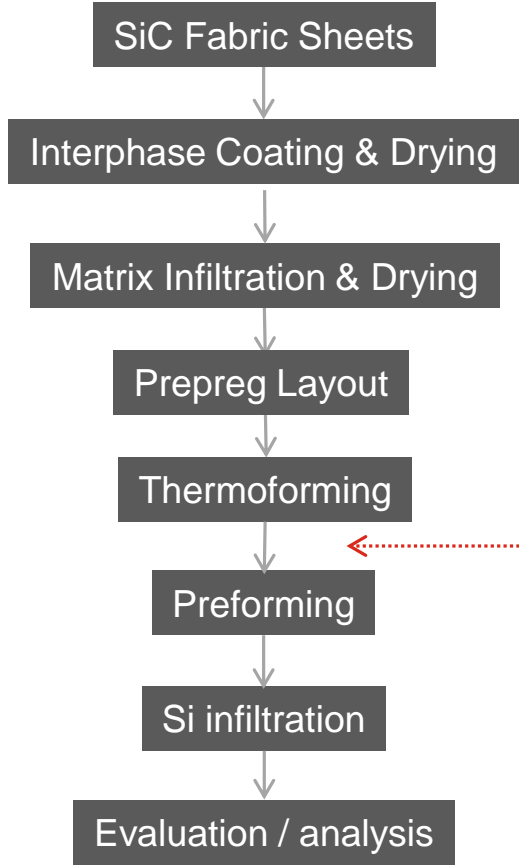
Fracture energy from crosshead position

$$\gamma = U / 2A$$

- Trapezium software (Shimadzu)



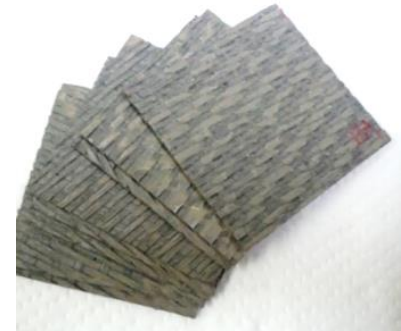
First Trial



Tyranno SA 8HS weave

BN ($\Phi 0.7 \mu\text{m}$) UHP in alcohol + resin

Matrix slurry (SiC + phenolic resin)



← Cured body

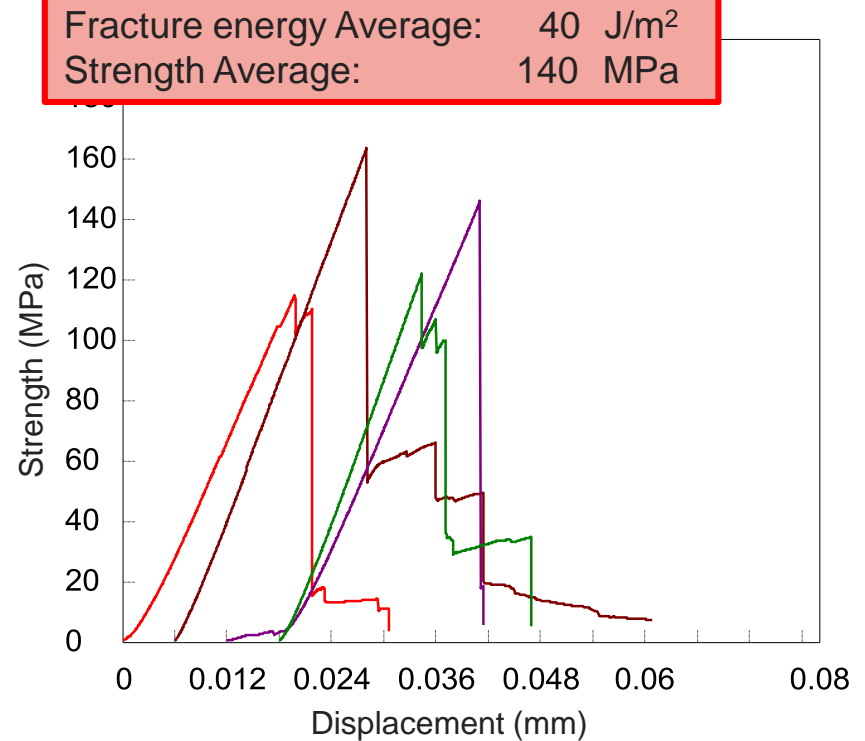
SENB (JCRS 201)
SEM, cross-sections



First Trial | Results

Density is high; porosity is low

	Vol.% Fiber	Density (g/cc)	Porosity (%)
Preform	43	2.19	15
Si Infiltrated	---	2.77	2



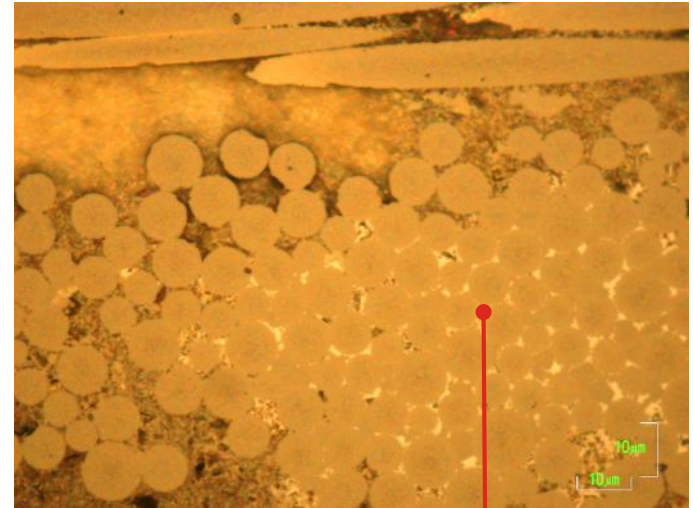
Both strength and breaking energy are low

First Trial | Observations & Conclusions

1. Silicon penetrated the fiber bundle
2. BN appears to be displaced or reacted with the silicon
> no fiber protection from the BN particles

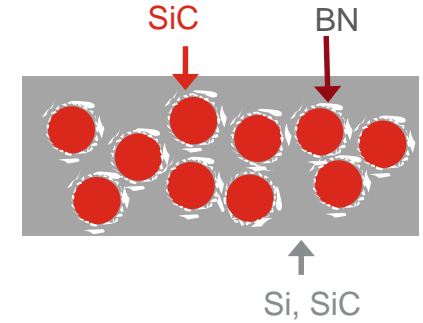
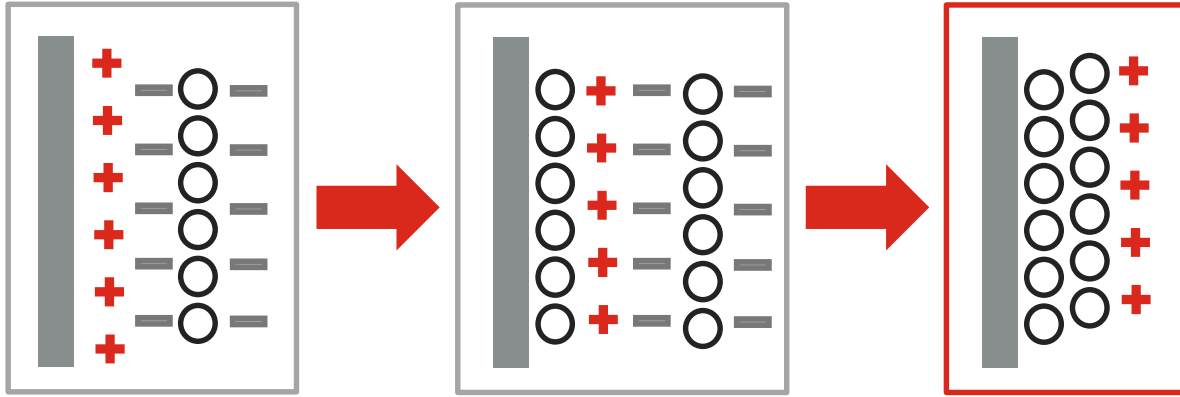
Strategies for improvement:

- a. Improve adhesion of BN to fibers
- b. Electrolyte solutions
- c. Thicker BN layers



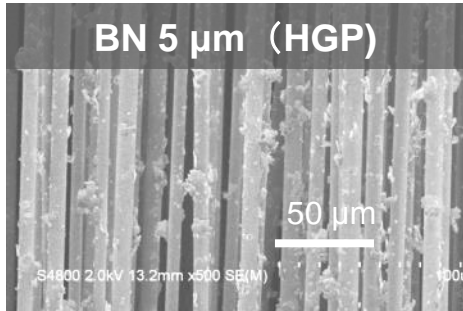
Bright areas indicate silicon
penetrated to interior of bundle.

Electrolyte Concept | Heterocoagulation

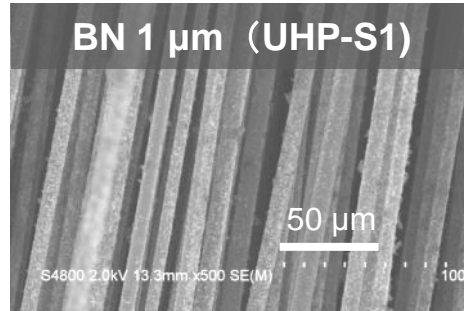
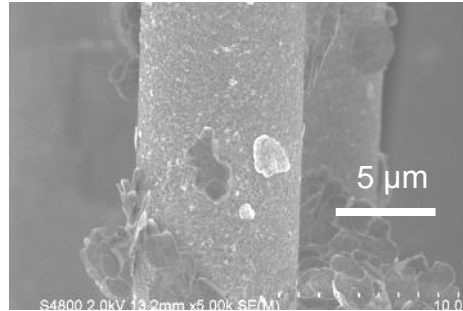


- Poly-electrolyte aqueous solutions: A- & B+
- Powder suspension made with A- electrolyte
- Fabric dipped in B+ electrolyte then in A-
- Coated fabric then rinsed with solution C

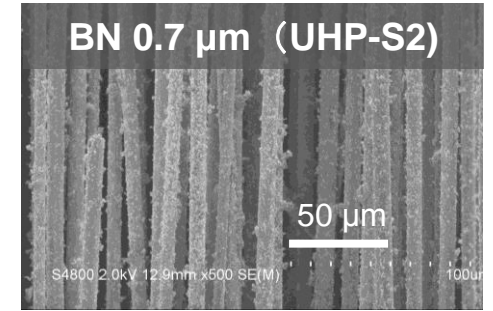
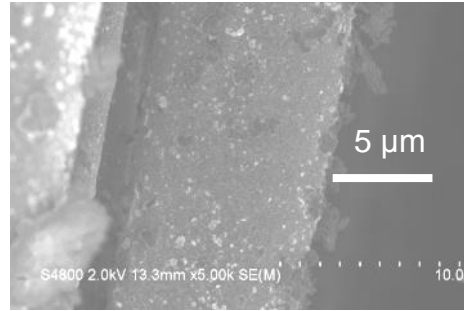
Particle Size Limitation



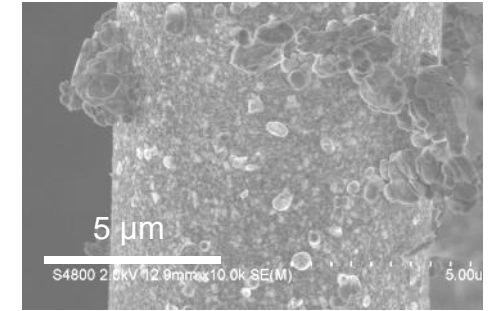
Not effective



Not effective at 1 μm

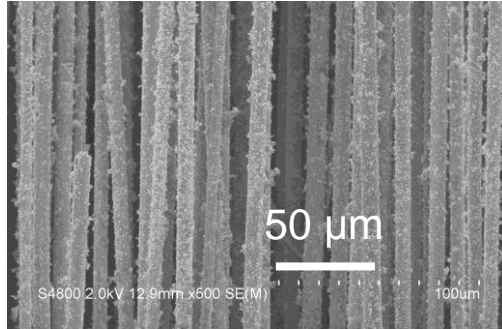


Very effective

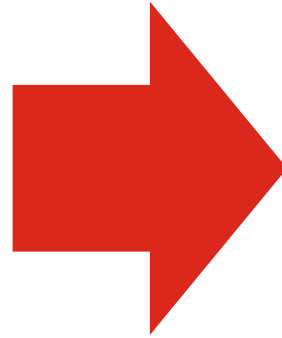
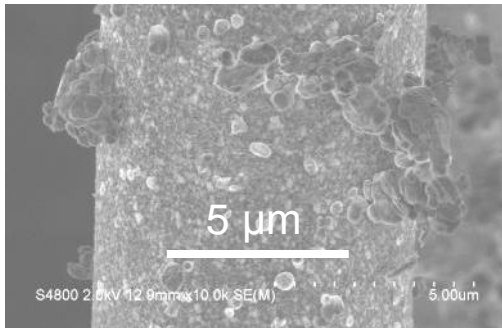


Improving Solution B

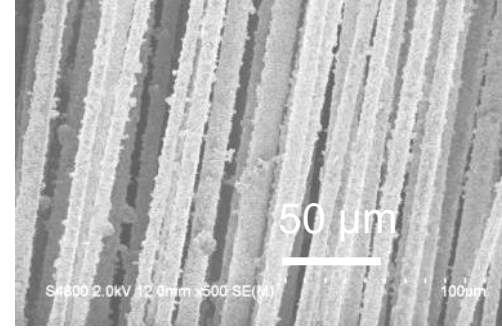
BN 0.7 μm (UHP)



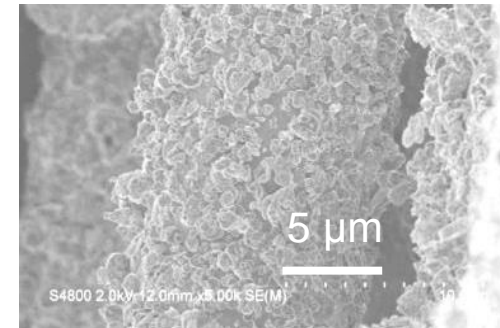
Single layer coat



BN 0.7 μm (UHP)



Improved process



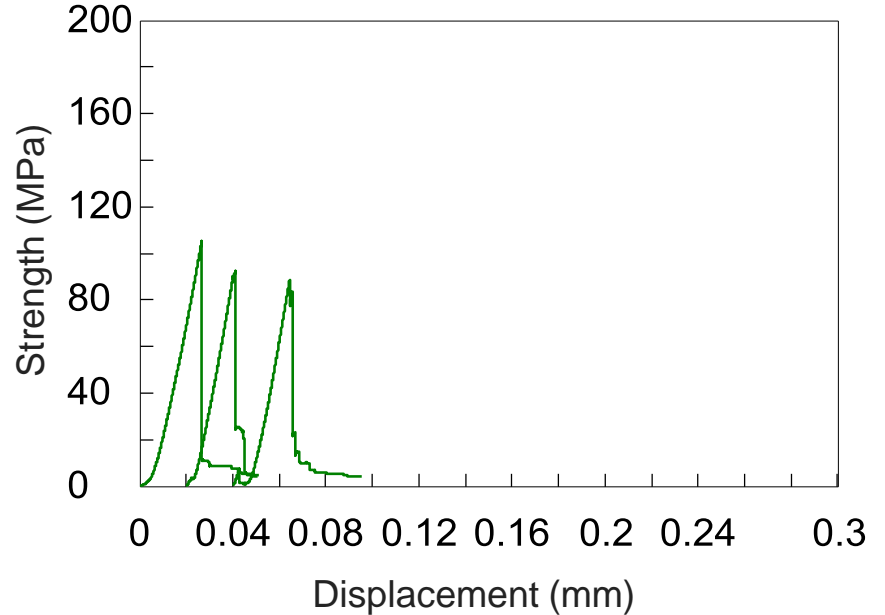
Heterocoagulation | Results

Parameter	Value
Vol % fibers	55
Density (g/cm ³)	2.88
Porosity (%)	3

Heterocoagulation trial

- All failures are brittle
- No improvement in strength
- No improvement in fracture energy

Fracture Energy, average	30 J/m ²
Strength, average	100 MPa



Modifying the MI Process

Issue

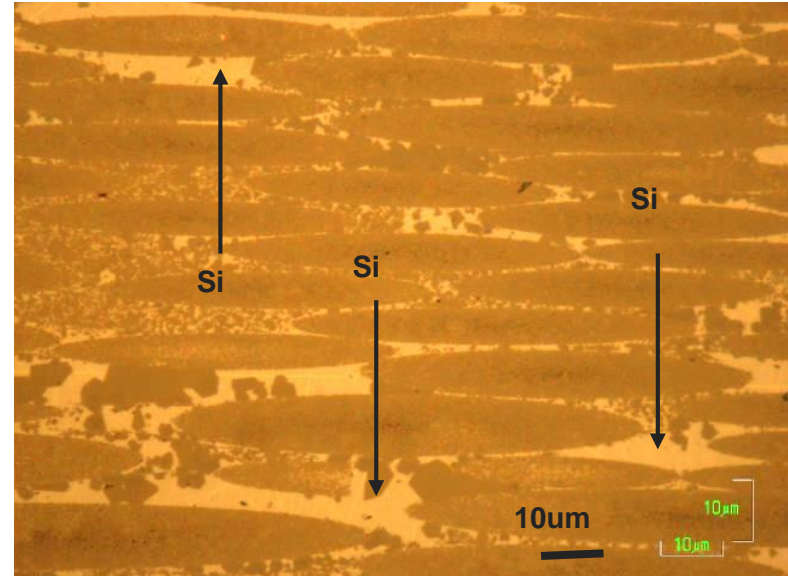
Excess silicon inside and in between fiber bundles

Goals

- Less interaction between Si(l) and BN coating
- Less fiber and interphase degradation
- Better mechanical properties

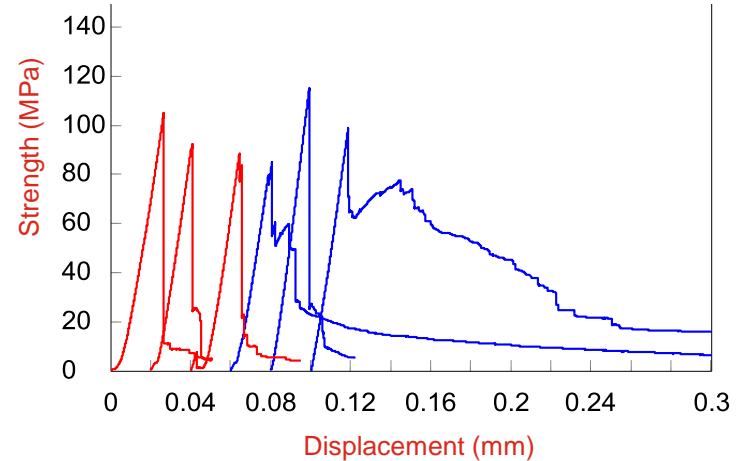
Approach

Reduce excess silicon by providing additional carbon for reaction during infiltration



Combining the Processes

PARAMETER	NO EXTRA RESIN	EXTRA RESIN
Vol.% Fibers	55	58
Density (g/cc)	2.88	2.82
Porosity (%)	3	2

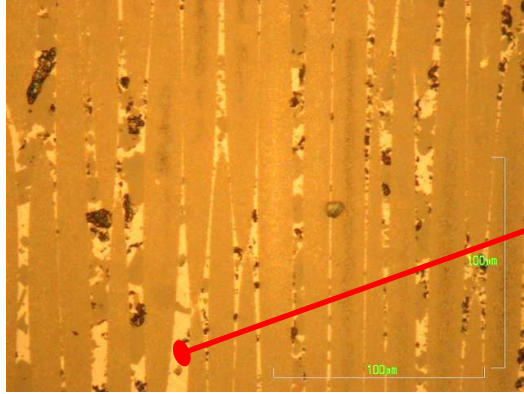


Extra resin (carbon) added

1. Significant increase in fracture energy ... but high variation
2. No strength improvement

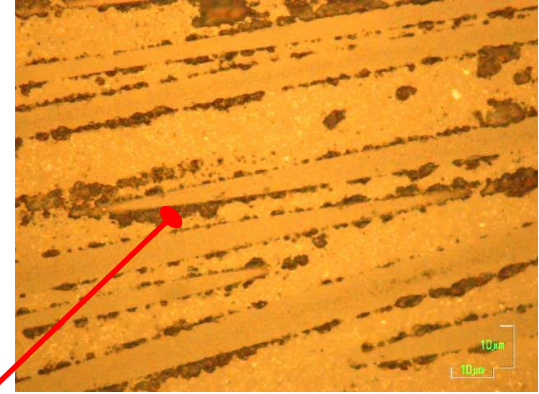
NO EXTRA RESIN	
Fracture Energy Average	30 J/m ²
Strength Average	100 Mpa
EXTRA RESIN	
Fracture Energy Average	200 J/m ²
Strength Average	100 MPa

Microstructures | With & Without Extra Carbon



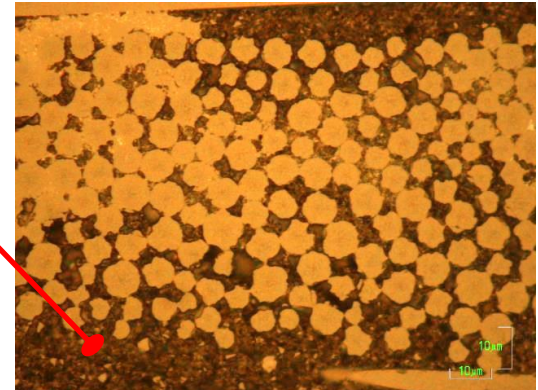
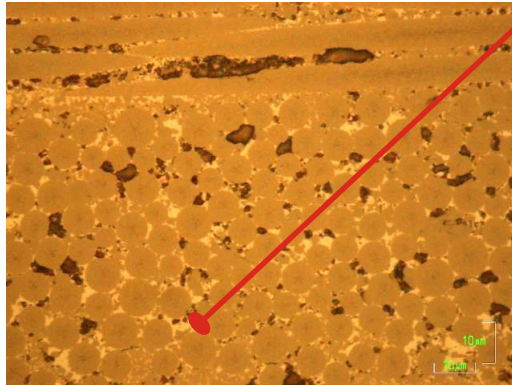
No extra carbon

Bright areas are silicon bonded to the fibers.



With extra carbon

Dark areas are silicon carbide next to the fibers.



Modifying Particle Coating Process

Issue

Fibers coated unevenly

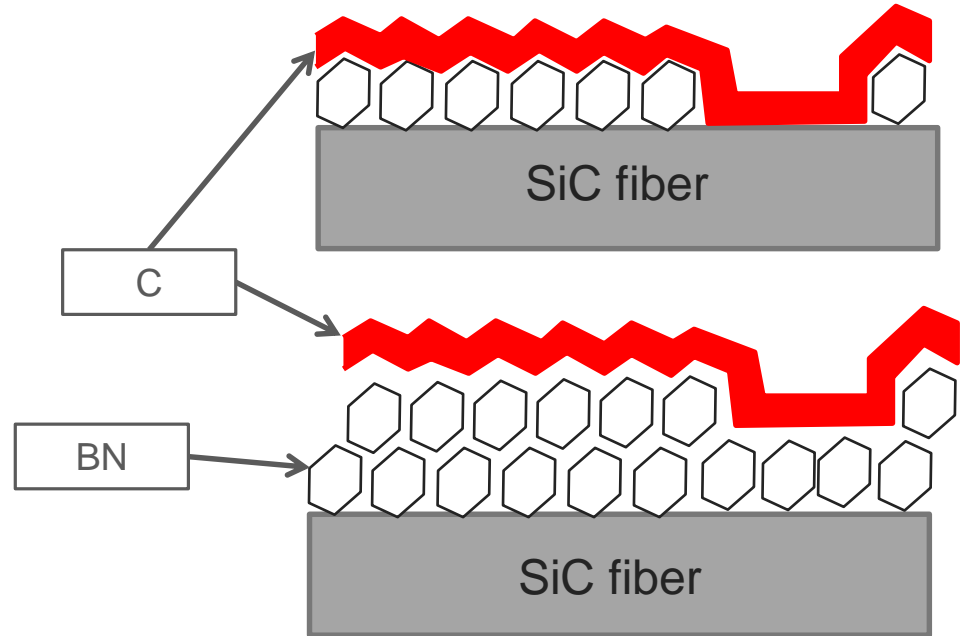
- Multiple layers in some areas
- No coating in some areas
- No fiber protection/weak interphase

Goals

- Improve coating uniformity
- Produce fiber/BN/C structure

Approach

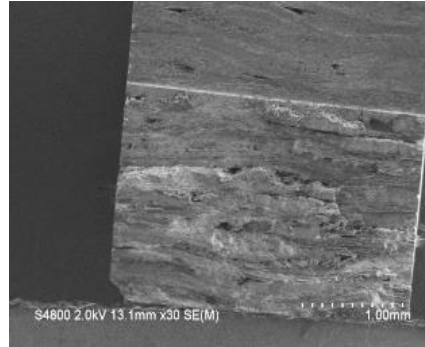
- Nano-sized BN particles
- Multiple BN coats



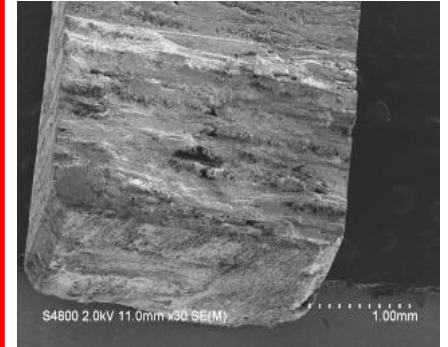
Fiber Pullout | Improves With Multiple Coats



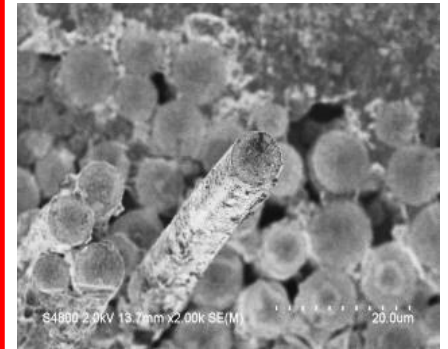
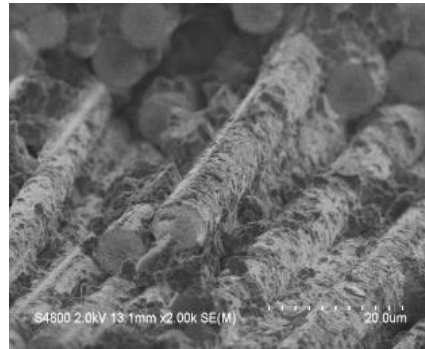
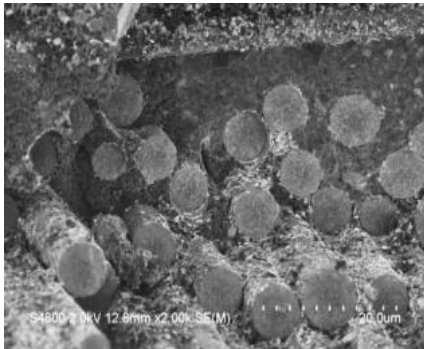
0.7 μm , 1X



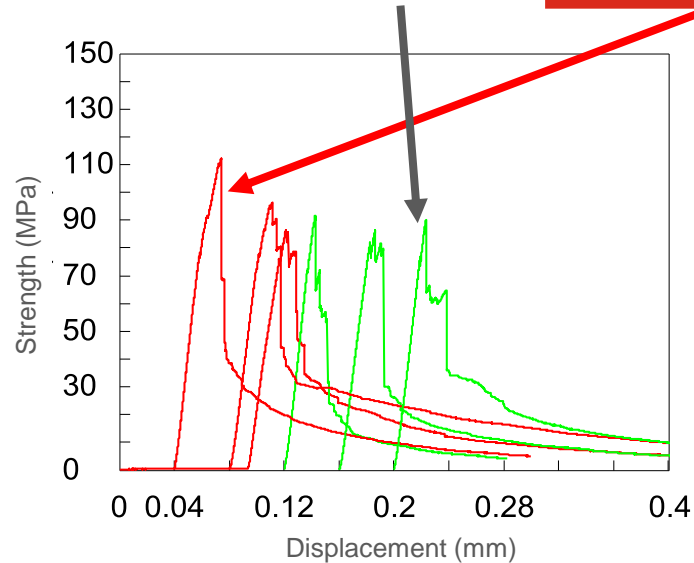
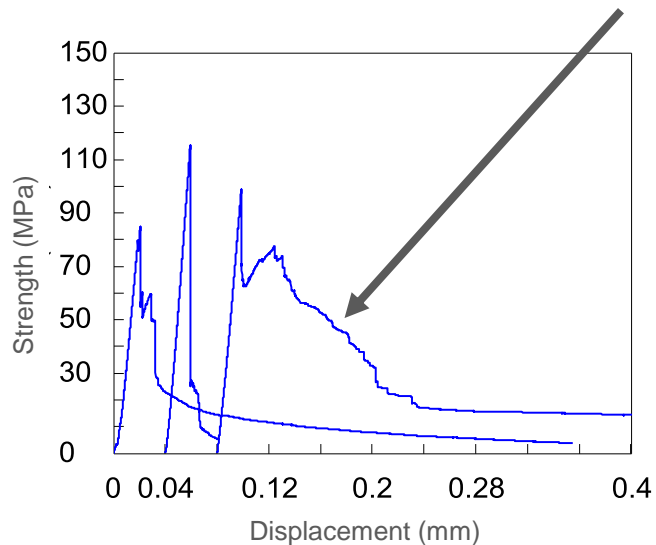
0.05 μm , 5X



0.05 μm , 7X



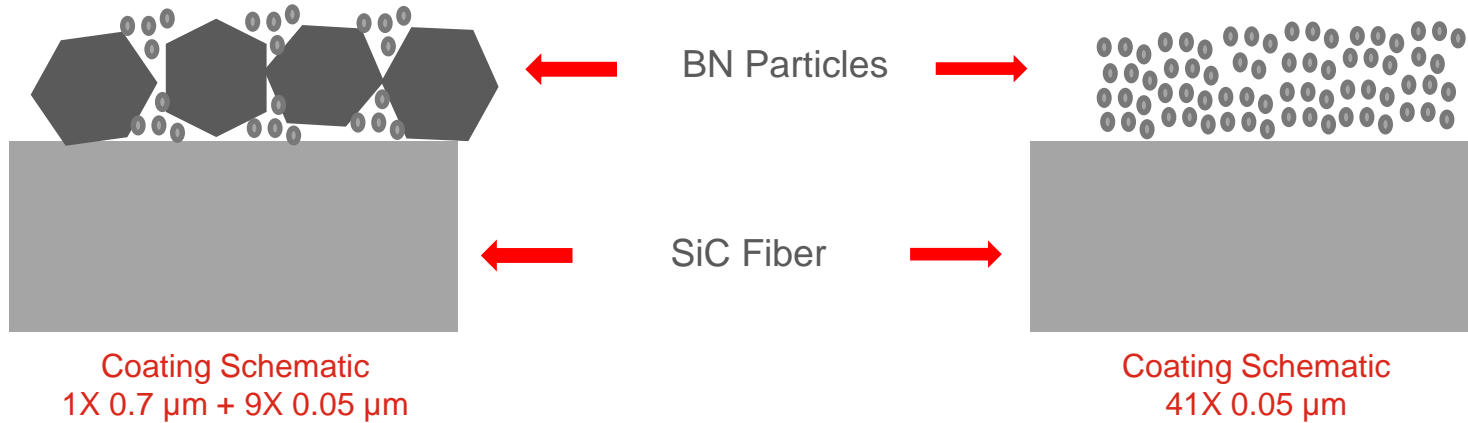
PARAMETER		1X BN (UHP) 0.7 μm	1X BN 0.05 μm	5X BN 0.05 μm	7X BN 0.05 μm
Vol. % Fibers		58	49	43	43
Bulk Density	(g/cm^3)	2.82	2.80	2.49	2.53
Porosity	(%)	2	5	11	12
Flex Strength	(MPa)	100	100	90	100
Fracture energy	(J/m^2)	200 (MAX 450)	70 (MAX 90)	100 (MAX 140)	150 (MAX 200)



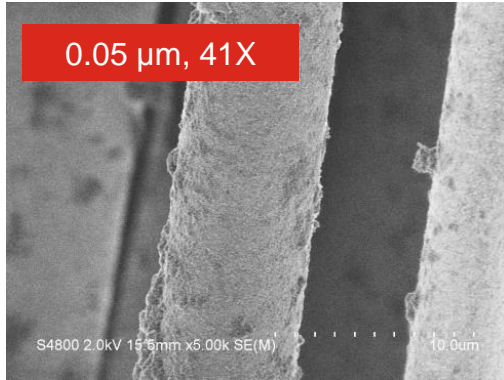
Scenarios to Increase Thickness

- Optimized particle packing;
bimodal distribution
- Minimize the number of layers

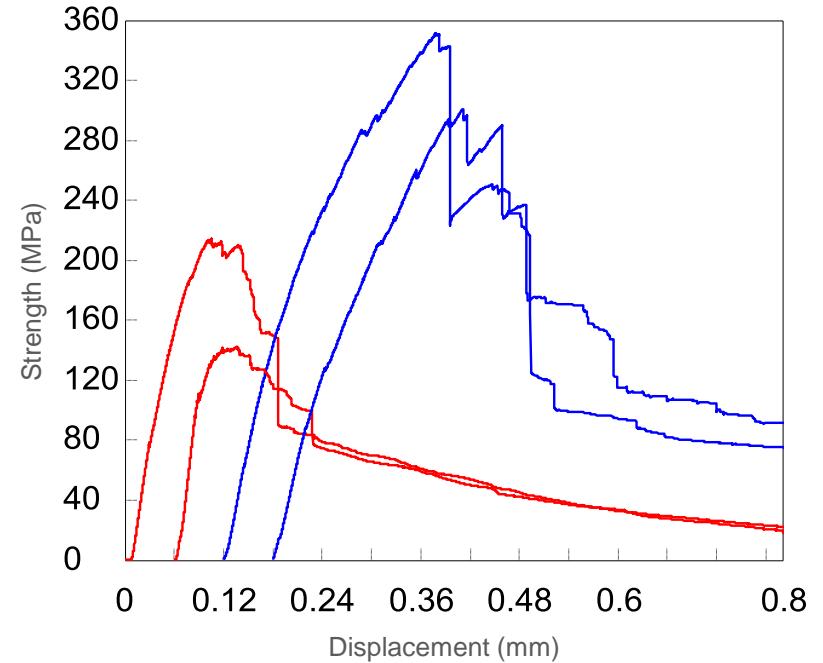
Multiple layers for thickness



Increase Number of Coatings



ITEMS		1 X 0.7 μm 9 X 0.05 μm	41 X BN 0.05 μm
Vol.% Fiber		48	49
Density	(g/cm ³)	2.60	2.62
Porosity	(%)	8.05	7.77
Strength	(MPa)	178	326
Avg Energy	(J/m ²)	1400	4000



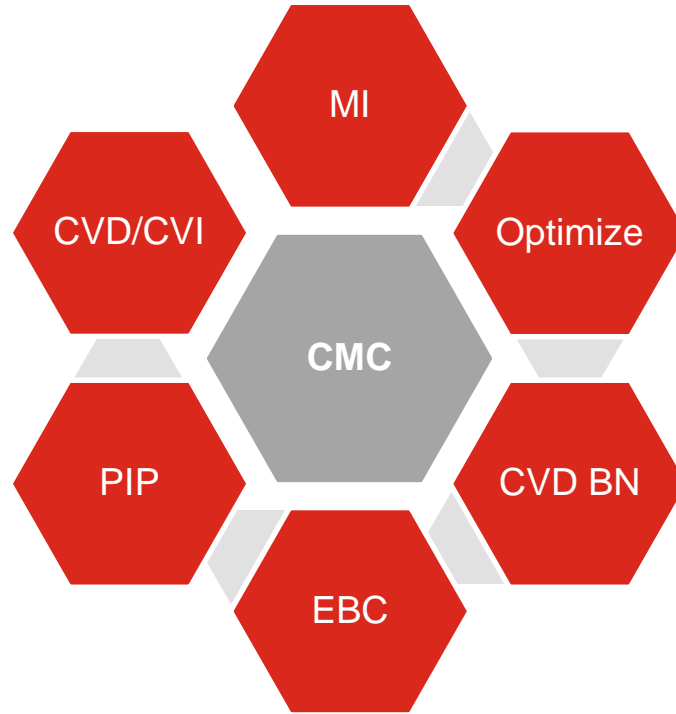
Conclusions

1. BN powder adhesion to SiC fiber by heterocoagulation
 - Coat with fine BN particles ($< 0.7 \mu\text{m}$)
 - Multiple coats applied
2. MI process improvement
 - Extra carbon added via resin
 - Coating over BN particles

Excellent mechanical properties achieved

- Strengths $> 300 \text{ MPa}$
- Fracture energy $> 4000 \text{ J/m}^2$

Next Steps



Thank You

November 8, 2017

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