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# Modelling study of two chemical looping reforming reactor configurations: Looping vs. switching

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# Modelling study of two Chemical Looping Reforming reactor configurations: Looping vs. Switching

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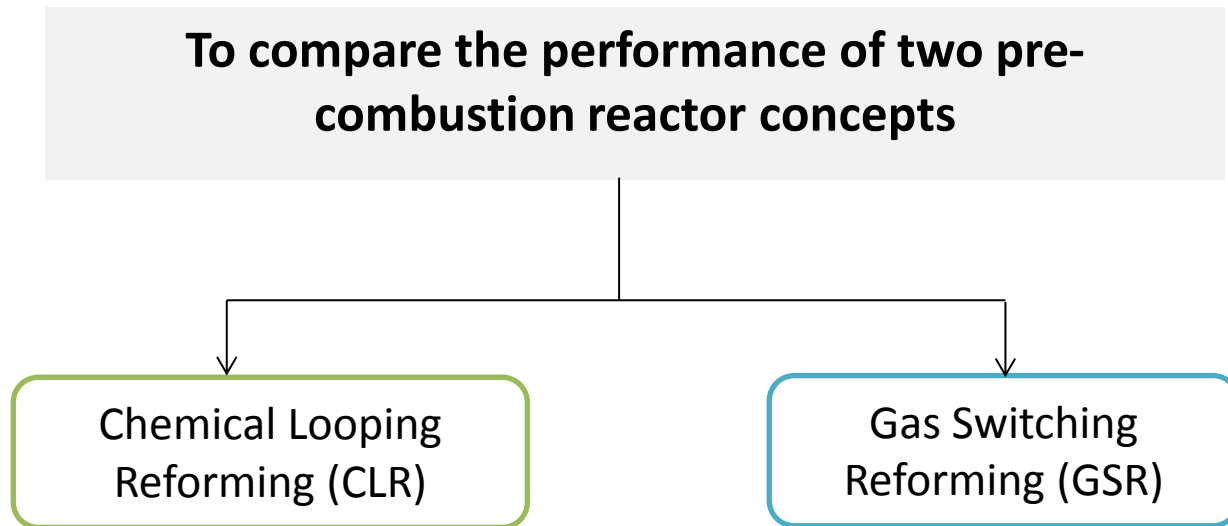
# Outline

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1. Objective
2. CLR vs. GSR principles
3. Simulations
4. Results and discussion
5. Conclusions

## 2. Objective of the work

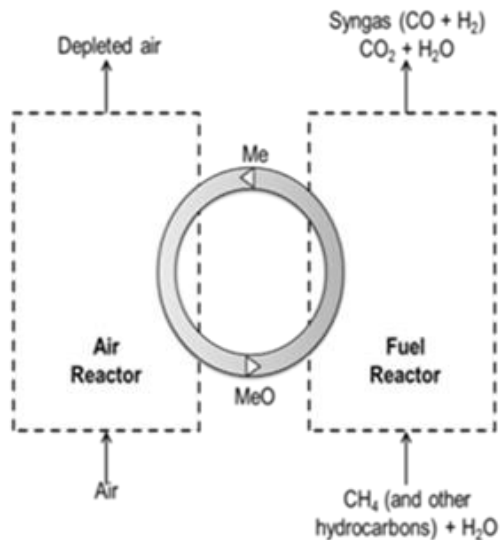
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# 3. CLR vs. GSR

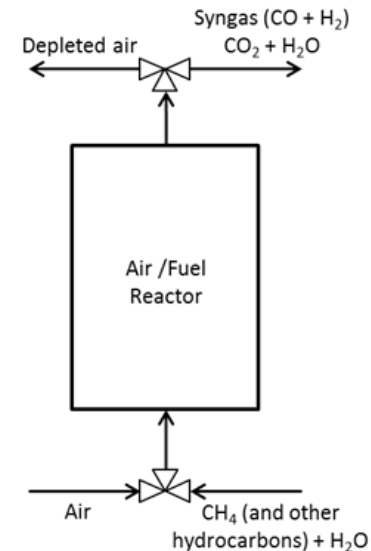
## CLR

- **Two interconnected FBR reactors** (AR and FR);
- **OC continuously transported** between AR and FR;
- **No mixing** between  $N_2$  and fuel;
- Scale-up and operational challenges.



## GSR

- **One FBR** for oxidation and reduction of the OC – **switching concept**;
- **Alternating feed** of air and fuel to the reactor unit;
- **Undesired mixing** between  $N_2$  and fuel;
- **Facilitates scaling-up** under pressurized conditions.



# 4. Simulations

Single formulation is used!

## 1-D phenomenological model for FBR

- **Generic formulation** based on the generic model developed by Abba *et al.* (2003)<sup>[1]</sup>;
- Uses an **averaging probabilistic approach** by Thompson *et al.* (1999)<sup>[2]</sup>;
- **Two-phase** model by Toomey and Johnstone (**L- and H-phases**)<sup>[3,4]</sup>;

### Differential Balances

- **Mass balance**
  - Gas total mass balance
  - Gas species mass balance for each phase
  - Total solids species mass balance
- **Total Energy balance**
- **Pressure Balance**



### Numerical scheme:

- Method of lines (MATLAB routine *ode15s*)
- Finite volume method (discretization in space)
  - **Non-uniform grid**
  - **Convective term:** 1<sup>st</sup> order upwind scheme
  - **Diffusion term:** central differences scheme

1. Abba, I.a., et al., *Spanning the flow regimes: Generic fluidized-bed reactor model*. AIChE Journal, 2003. **49**: p. 1838-1848.
2. Thompson, M.L., H. Bi, and J.R. Grace, A generalized bubbling / turbulent fluidized-bed reactor model. *Chemical Engineering Science*, 1999. **54**: p. 3-10.
3. Kunii, D. and O. Levenspiel, *Fluidization Engineering*. second ed. 1991: Butterworth-Heinemann.
4. Mahecha-Botero, A., et al., *Pure hydrogen generation in a fluidized bed membrane reactor: Application of the generalized comprehensive reactor model*. *Chemical Engineering Science*, 2009. **64**(17): p. 3826-3846.

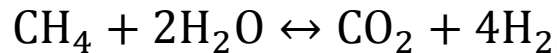
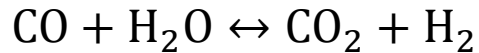
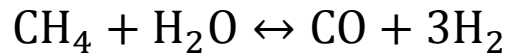
# 4. Simulations

## Reactions and Kinetics

### Reforming stage

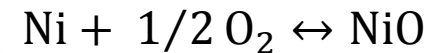
#### Reforming<sup>[1]</sup>

Ni as catalyst



Fuel Reactor

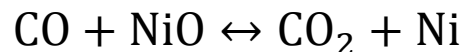
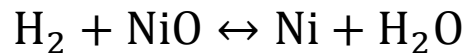
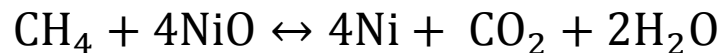
#### Oxidation of the oxygen carrier<sup>[2]</sup>



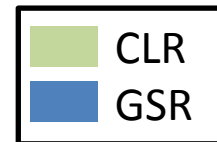
Air Reactor

Oxidation stage

#### Reduction of the oxygen carrier<sup>[2]</sup>



Reduction stage



- Xu, J. and G.F. Froment, *Methane steam reforming, methanation and water-gas shift: I. Intrinsic kinetics*. AIChE Journal, 1989. **35**(1): p. 88-96.
- Abad, A., et al., *Mapping of the range of operational conditions for Cu-, Fe-, and Ni-based oxygen carriers in chemical-looping combustion*. Chemical Engineering Science, 2007. **62**(1-2): p. 533-549.

# 4. Simulations

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## Simulation Parameters

Steam flowrate	170 ton/h
Fuel flowrate	250 ton/h
Maximum temperature	1100 °C
Fuel inlet temperature	205 °C
Steam inlet temperature	400 °C
Operating pressure	17.3 bar
OC density	3446 kg/m <sup>3</sup>
Particle diameter	250 μm
Reactor diameter	6 m
Reactor height	7 m
Axial resolution	20 cells

How to compare these two technologies?

Same simulation parameters and physical properties

**Study variable: Degree of Oxygen Carrier utilization**



How to adjust this parameter?



# 4. Simulations

**CLR: Oxygen carrier flux**

↓ OC flux: ↑ OC residence time

**GSR: Cycle time flux**

↑ cycle time: ↑ reduction + ↑ oxidation

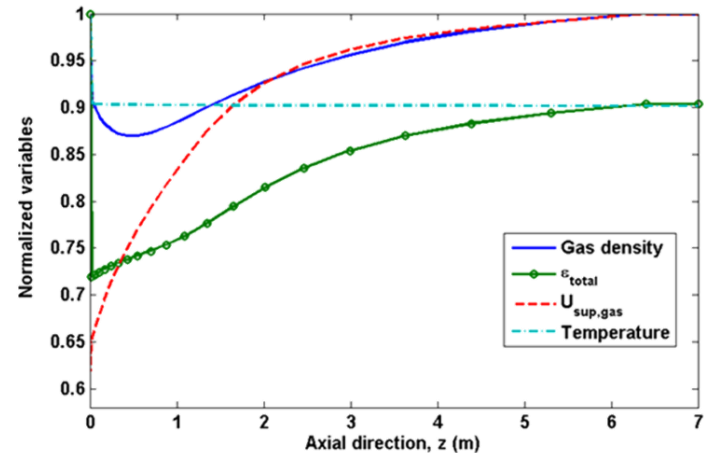
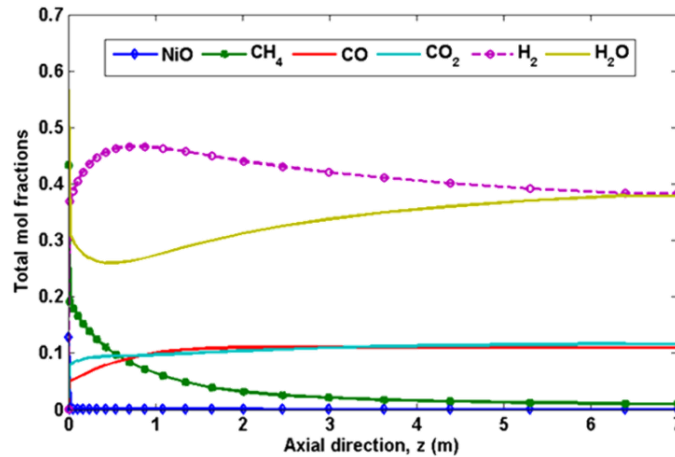


Higher oxygen carrier conversion

Degree of OC utilization (%)	CLR	GSR		
	OC flux (kg/m <sup>2</sup> s)	Oxidation stage time (s)	Reduction stage time (s)	Reforming stage time (s)
10	466	25	13	25
20	233	68	34	68
40	116.5	198	99	198
60	82.4	400	200	400
80	58.25	-	-	-

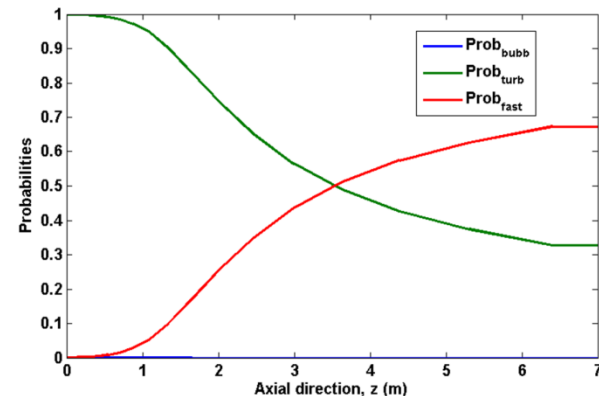
# 5. Results: Profiles

## Chemical Looping Reforming: Fuel Reactor



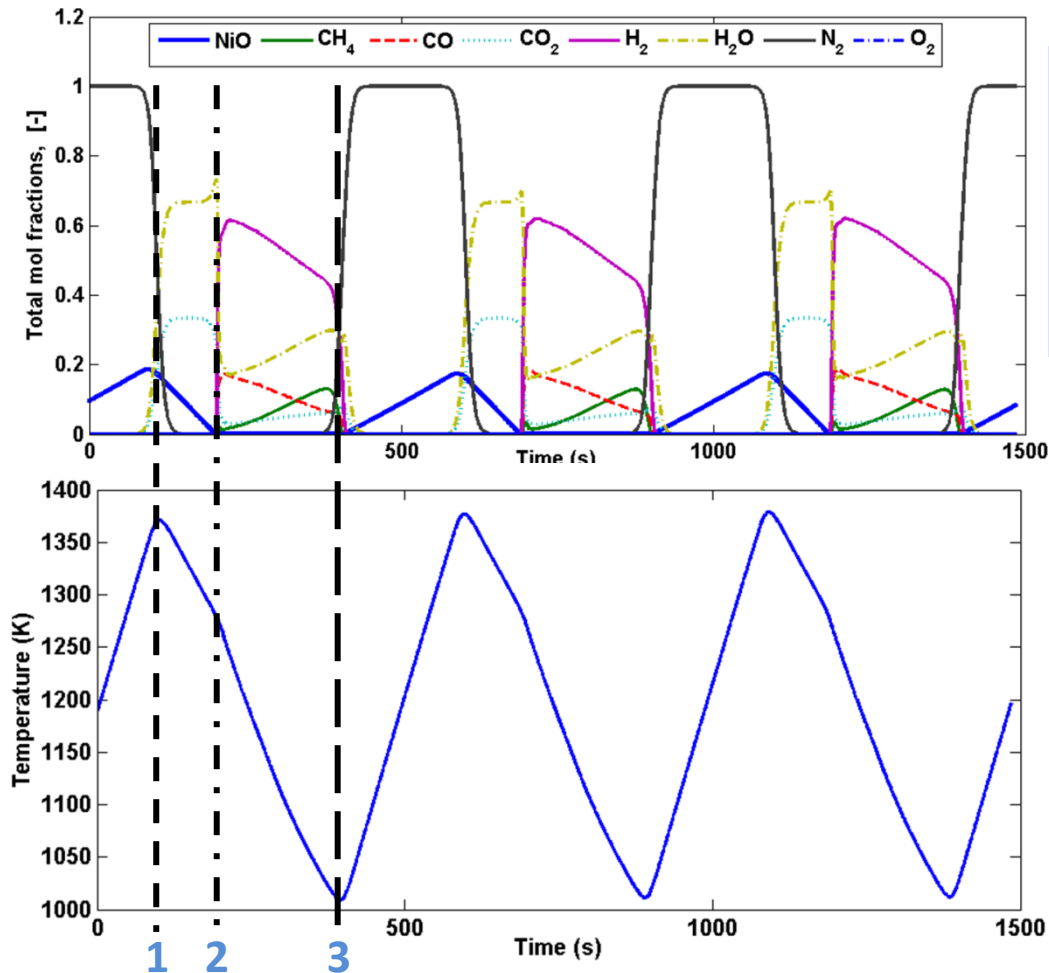
Maximum values: 2.94 kg/m<sup>3</sup> for the gas density, 1 for the void fraction, 2.4 m/s for the superficial velocity and 989 °C for the temperature

- Reforming reactions dominate at the beginning of the reactor → system far from equilibrium conditions → production of H<sub>2</sub> → density decrease
- Reduction reactions dominate at the end;
- Low amount of NiO through the bed;
- Temperature almost constant → good axial mixing

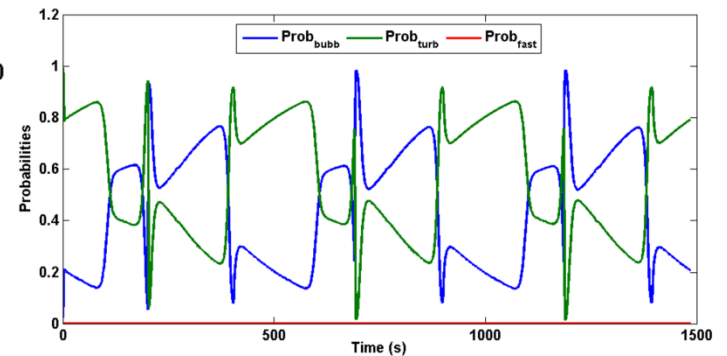


# 5. Results

## Gas Switching Reforming



- O<sub>2</sub> totally consumed in the oxidation stage;
- Undesired mixture of N<sub>2</sub> with fuel → reduces CO<sub>2</sub> capture performance;



1. Oxidation
2. Reduction
3. Reforming

# 5. Results

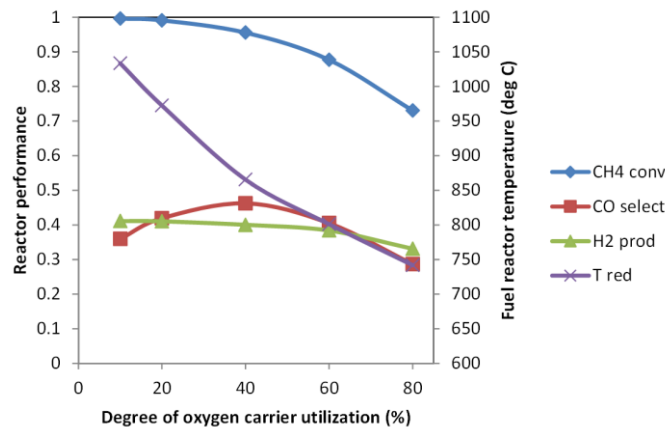
## Performance Measures

CH<sub>4</sub> conversion

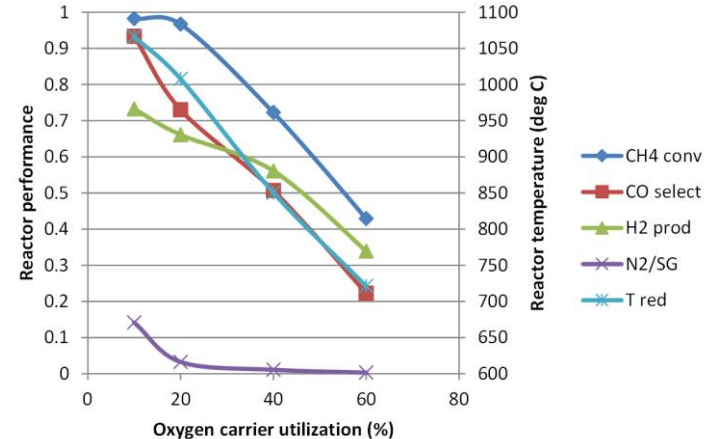
CO selectivity

H<sub>2</sub> production performance

CLR



GSR



### Higher OC utilization

- Lower reduction temperature → low CH<sub>4</sub> conversion (by reforming endothermic reactions) → productivity of H<sub>2</sub> decreases
- Lower CO selectivity → WGS reaction

### Lower OC utilization

- Lower CO selectivity → To supply heat

### Higher OC utilization

- Lower CH<sub>4</sub> conversion → Reforming stage is higher
- Lower H<sub>2</sub> productivity → lower CH<sub>4</sub> conversion

### Lower OC utilization

- Higher amount of N<sub>2</sub> mixed with fuel → Short cycle times

# 6. Conclusions

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## 1. CLR

- Lower degree of OC utilization (higher OC circulation rate) → higher temperature in fuel reactor → better reforming performance
- However, high OC circulation rate can bring practical and economic challenges

## 2. GSR

- Lower degree of OC utilization (shorter stage times) → higher temperature in reforming stage → higher CH<sub>4</sub> conversion and H<sub>2</sub> production
- However, undesired mixing of N<sub>2</sub> with CO<sub>2</sub> and syngas increases with shorter stage times

# 6. Conclusions

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## 3. CLR vs. GSR

- H<sub>2</sub> production and CO conversion is higher in GSR
- Fuel conversion is higher for CLR with higher CO<sub>2</sub> content
- CLR is best suited to thermal power production with pre-combustion CO<sub>2</sub> capture and GSR to pure H<sub>2</sub> production

Thank you for your Patience!!!

**Questions?**