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Mechanical stability limits of bi-layer thermal barrier coatings

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[1] R.A. Miller, J.L. Smialek, and R.G. Garlick, in Science and Technology of Zirconia, A. H. Heuer and L. W. Hobbs, Eds., Columbus, OH, USA: The American Ceramic Society, (1981) 241-253. [2] R. Subramanian, A. Burns, and W. Stamm, in Proceedings of ASME Turbo Expo 2008: Power for Land, Sea and Air, ASME, (2008). [3] R. Vaßen, F. Traeger, and D. Stöver, International Journal of Applied Ceramic Technology, vol. 1, no. 4 (2004) 351-361

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Research for Sustainable Technologies



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Mechanical Stability Limits of Bi-Layer Thermal Barrier Coatings

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Materials
Chemical Engineering
Biotechnology

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**E. Bakan
R. Vaßen**

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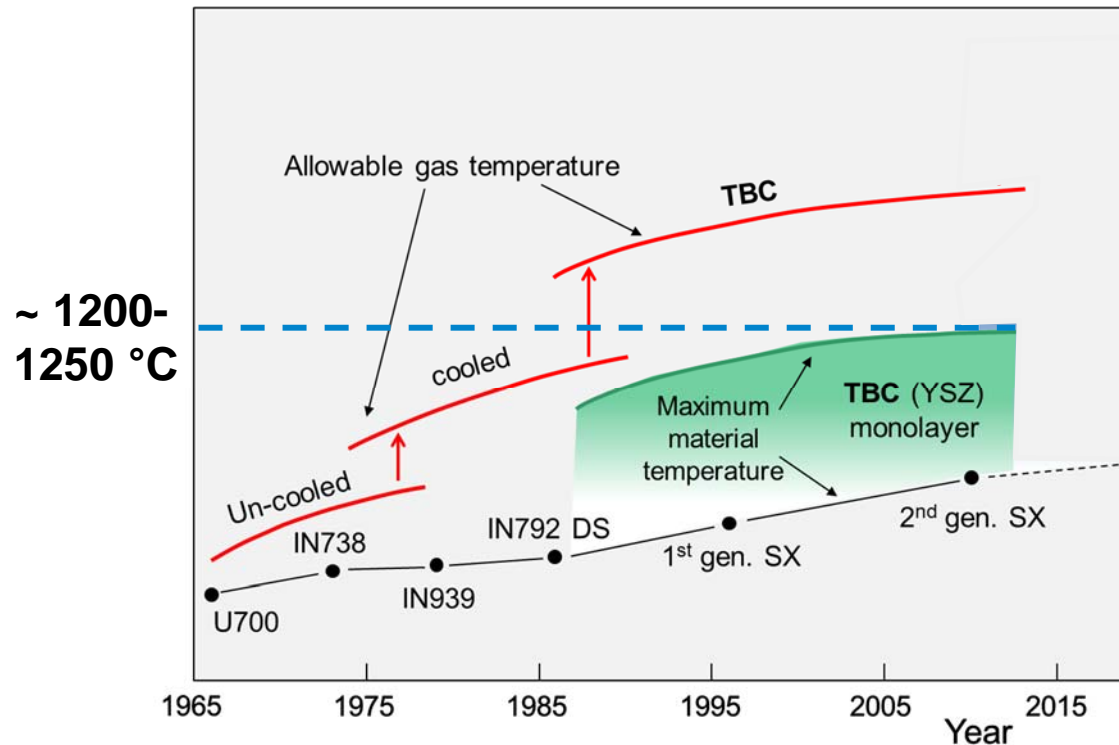


Rolls-Royce®



Motivation

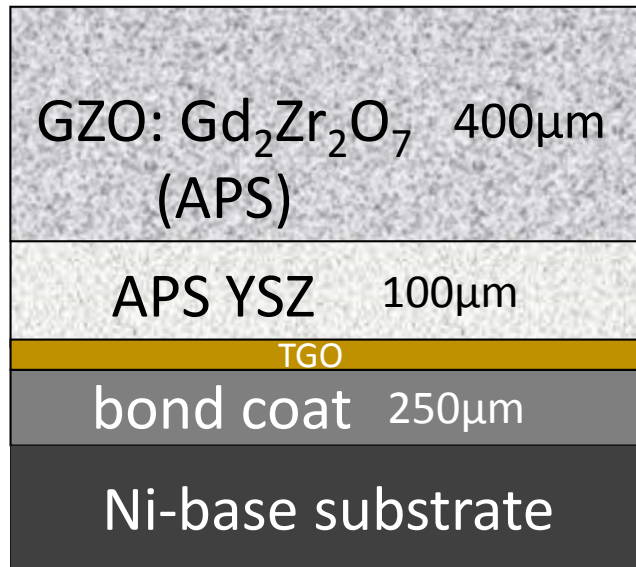
Ongoing effort to increase operating temperature / efficiency



However, the temperature limit of 7YSZ is around 1250°C due to phase transformations above this temperature [1]
→ Search for new materials / new TBC solutions

[1] W. Pan et al., MRS BULLETIN , Vol. 37 (2012)

Approach – Bi-Layer TBC



Bi-Layer Concept:

- surface temperatures > 1250 °C
- crack resistance to TGO growth induced stresses
- avoiding unwanted reactions between GZO and TGO



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DARMSTADT



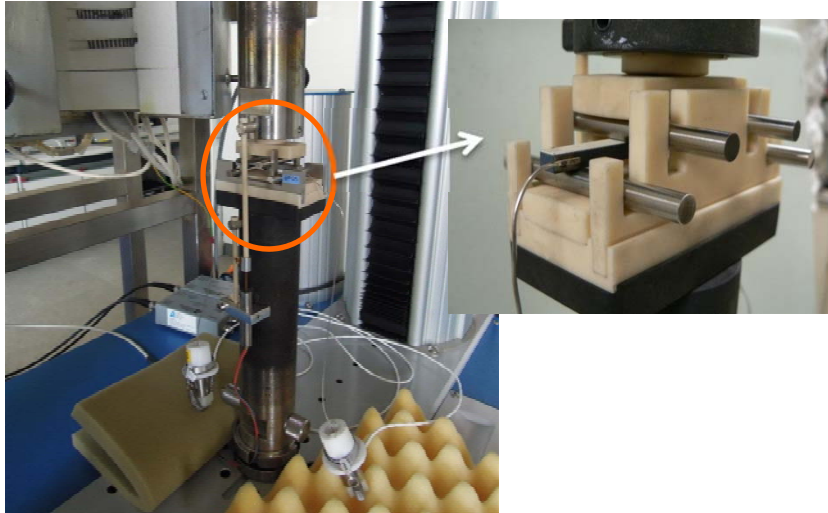
- Optimization of spray process
- Sample manufacturing

- Oxidation testing
- Mechanical testing (Charalambides test, G_{ic})
- TGMF testing

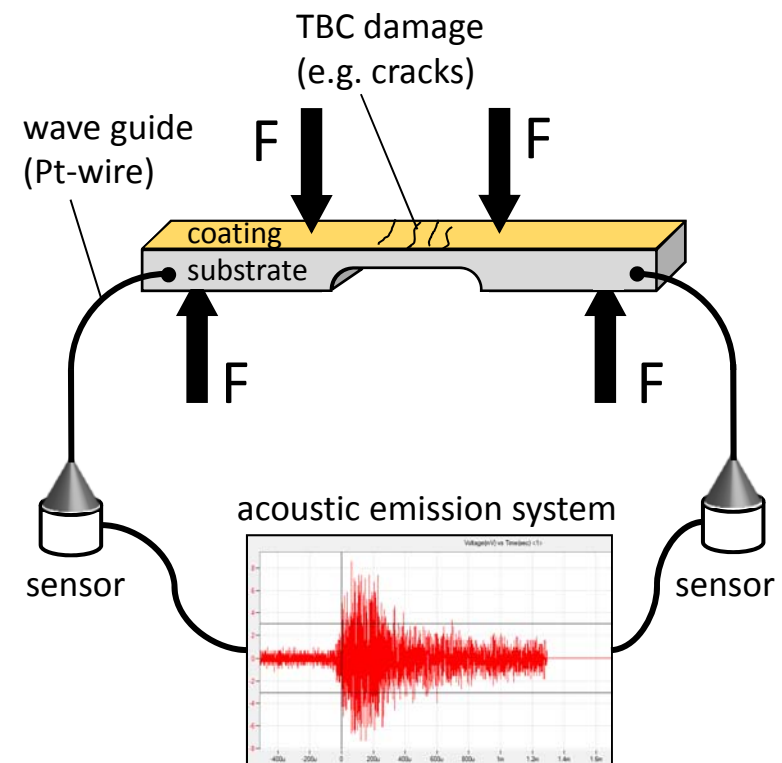
- Oxidation testing
- Mechanical testing (4-point bending test, ϵ_c)
- Lifetime modeling

4-pt. Bending with Acoustic Emission Measurement

4-Point Bending



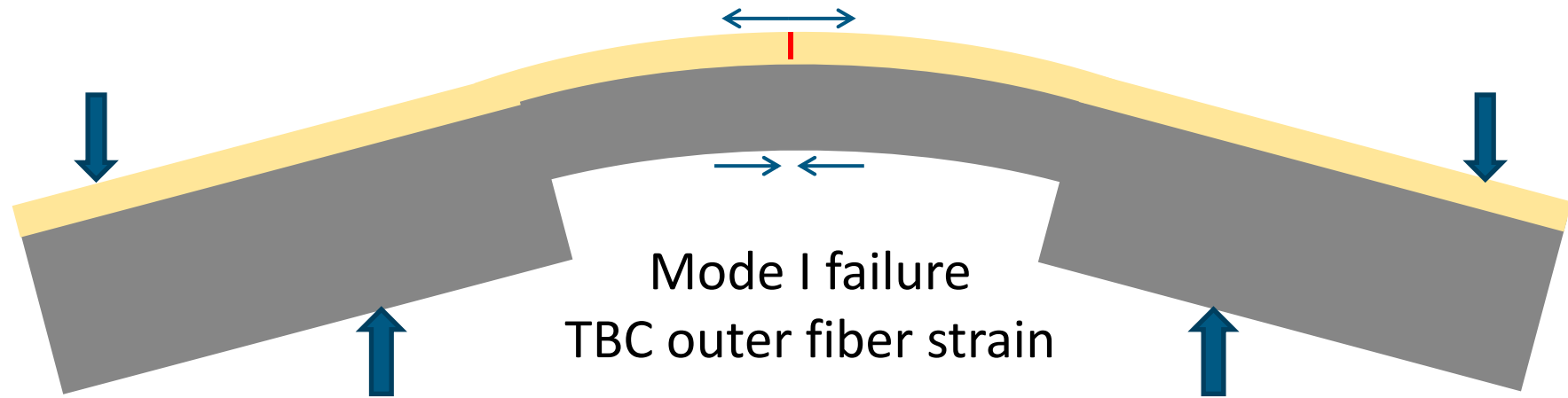
50kN
Universal Testing
Machine



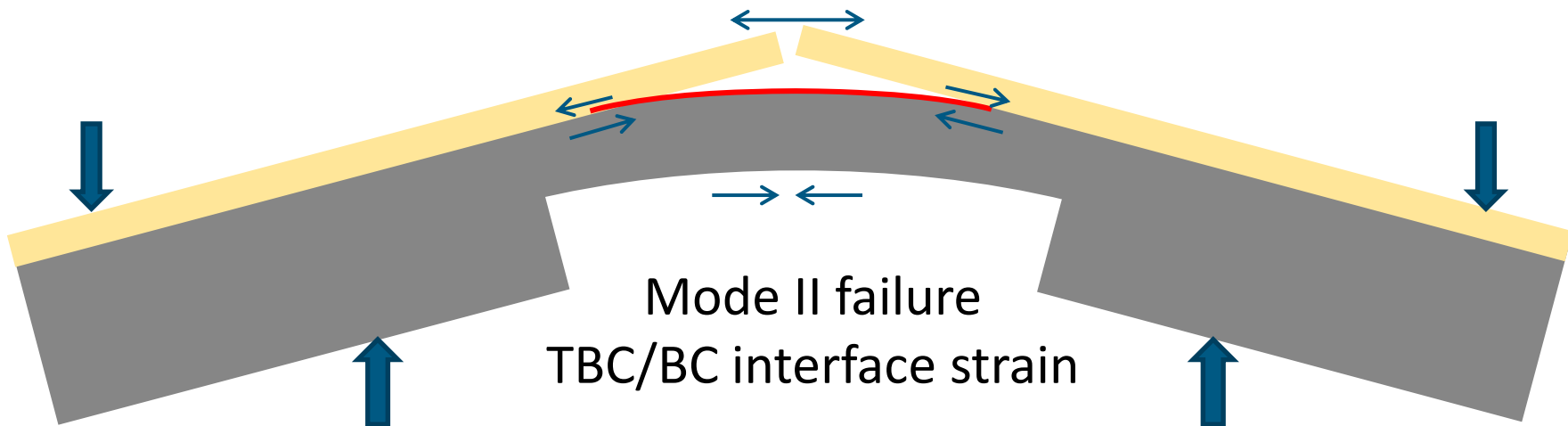
Testing was performed at RT

4-Point Bend Testing – TBC in Tension

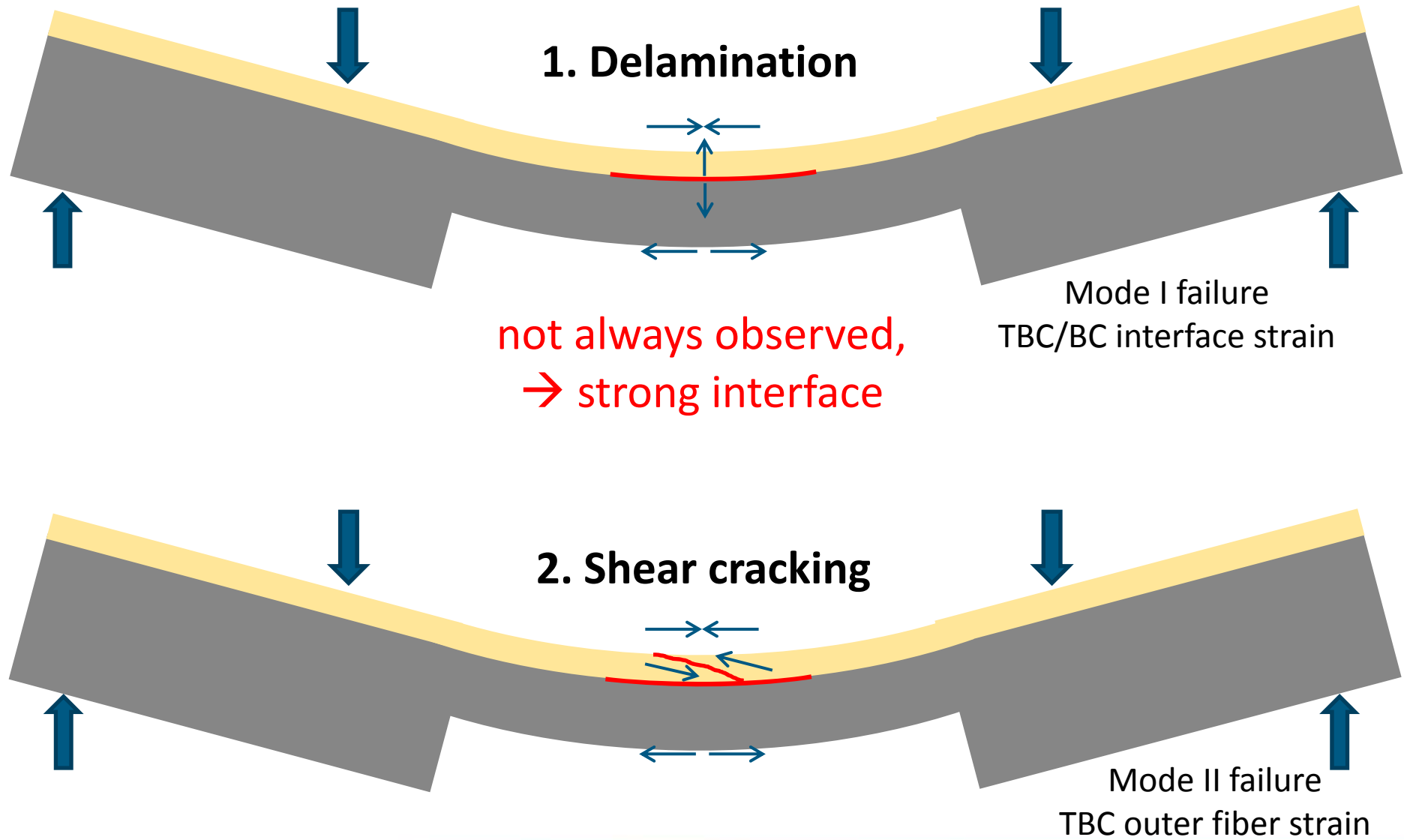
1. Segmentation



2. Delamination



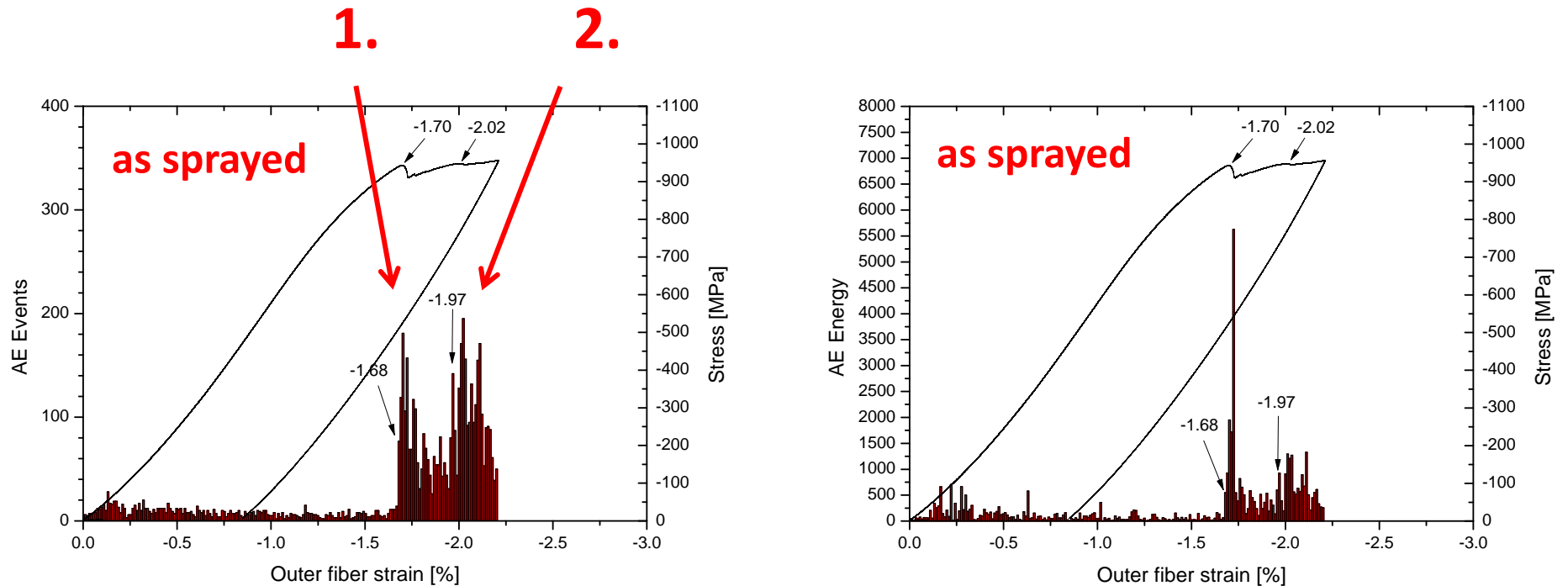
4-Point Bend Testing – TBC in Compression



Compressive Loading of TBC, Bi-Layer System

4-PB Results - Compression

Two distinct peaks can be identified in the acoustic emission signal under compressive loading!

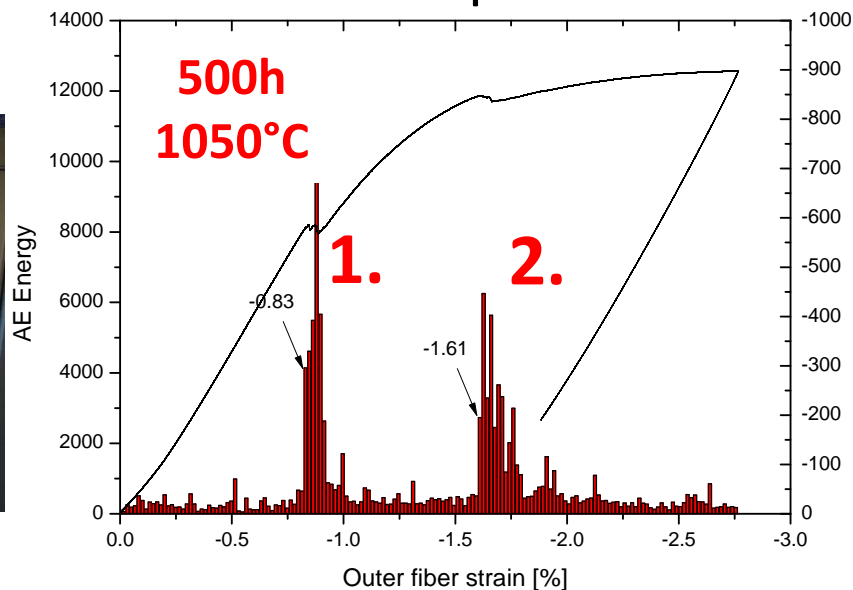
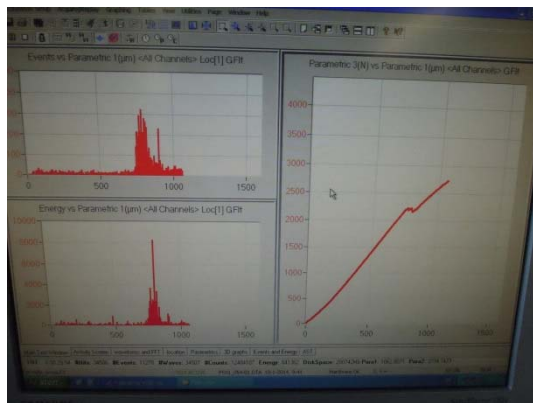


What are the individual peaks?

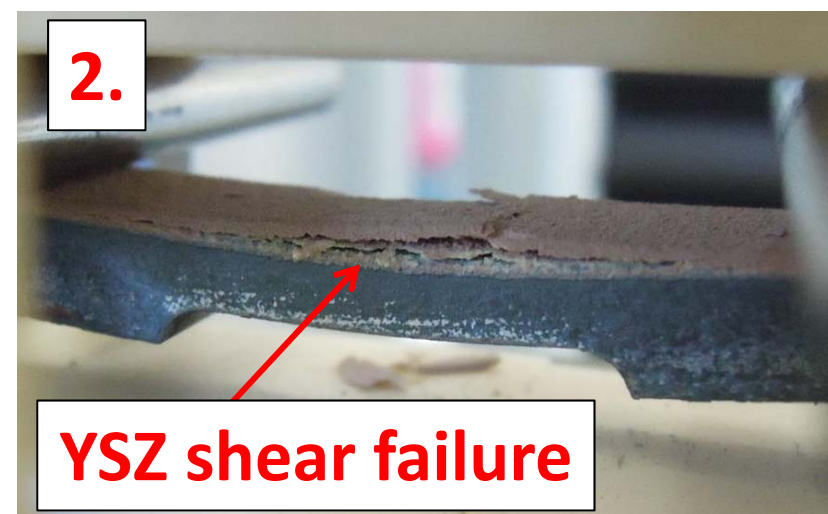
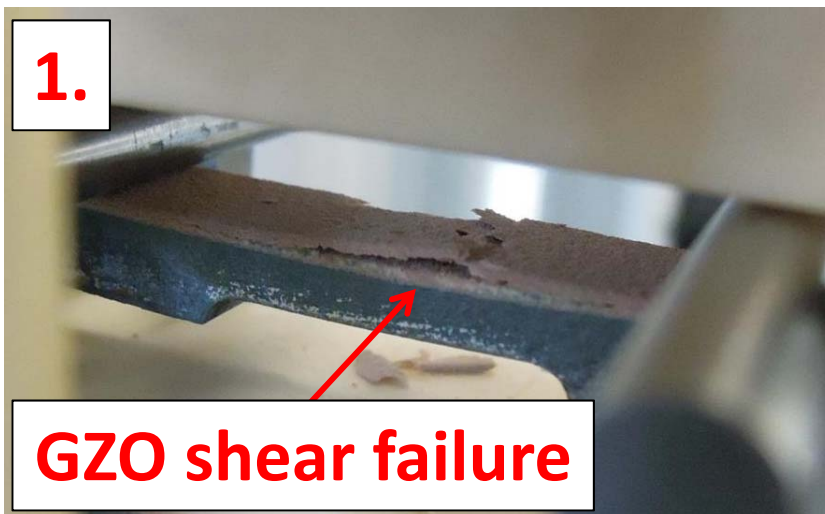
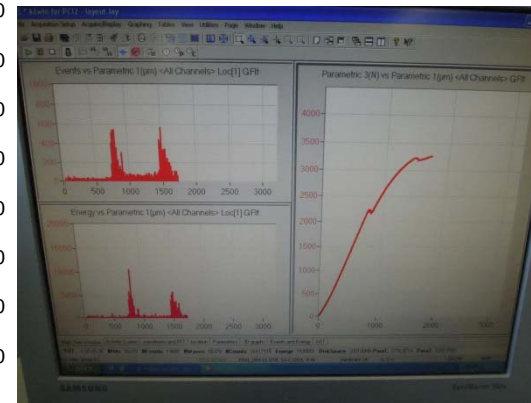
4-PB Results - Compression

4-PB in compression

1.

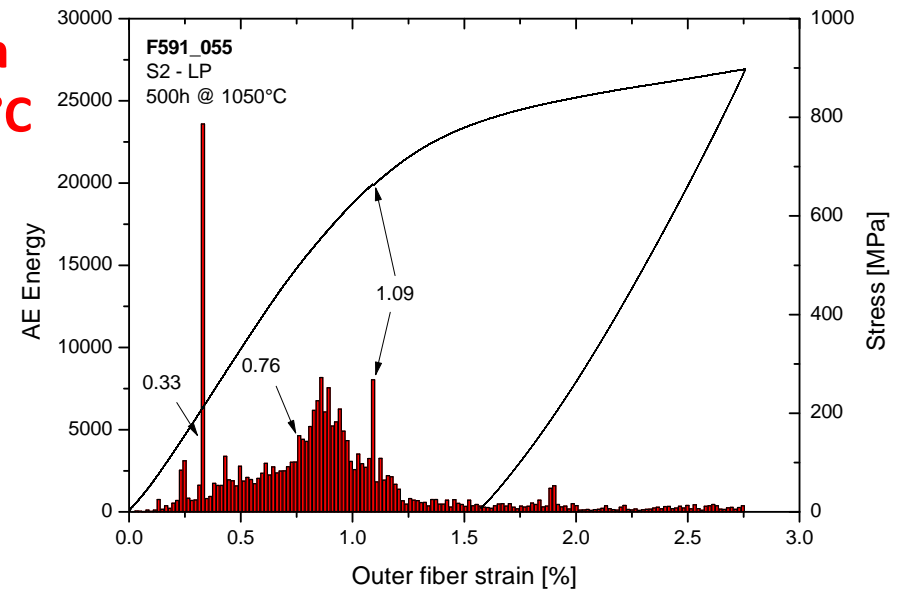
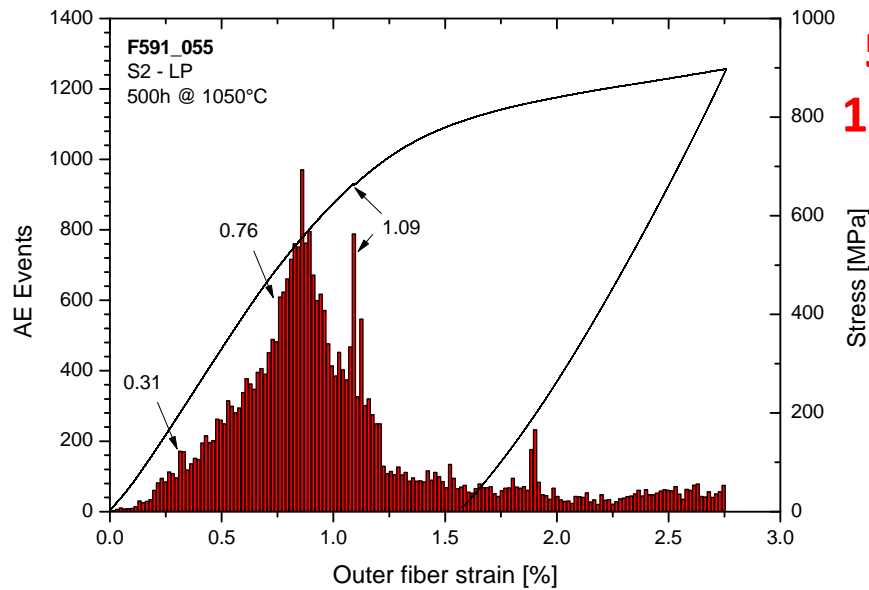


2.



Tensile Loading of TBC, Bi-Layer System

4-PB Results - Tension

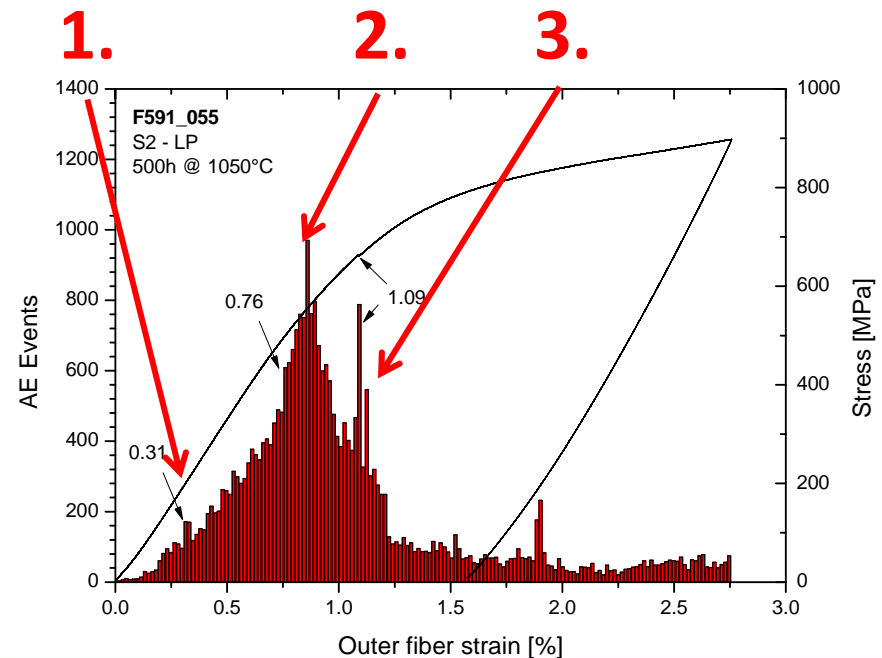
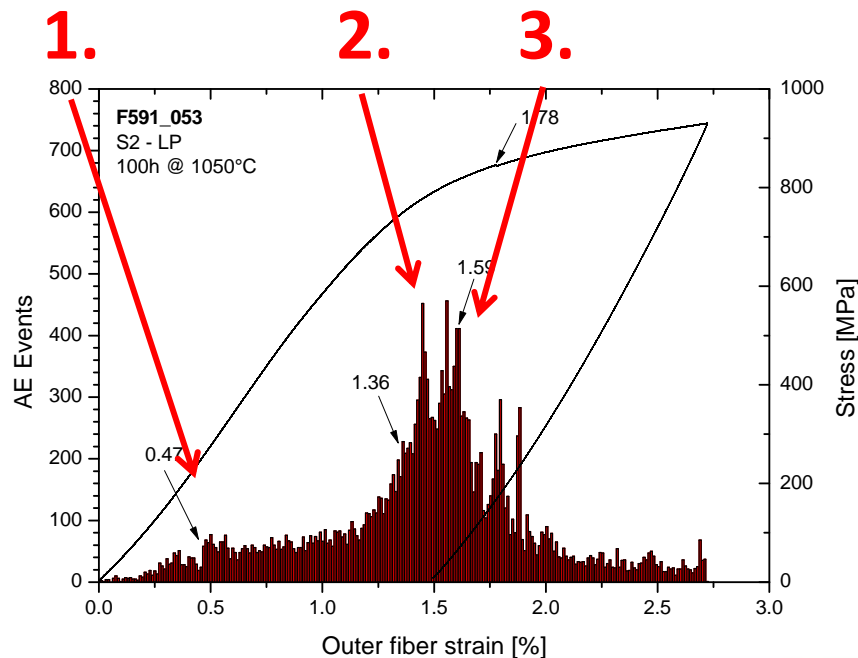


4-PB Results - Tension

What are the individual peaks?

- Tensile geometry does not lead to well separated peaks
- Some samples show gradually increasing AE signal at the beginning

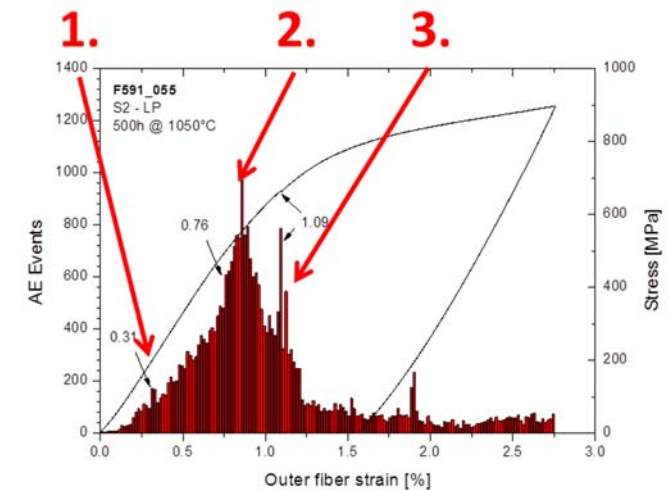
However, maybe 3 signals can be identified:



4-PB Results - Tension

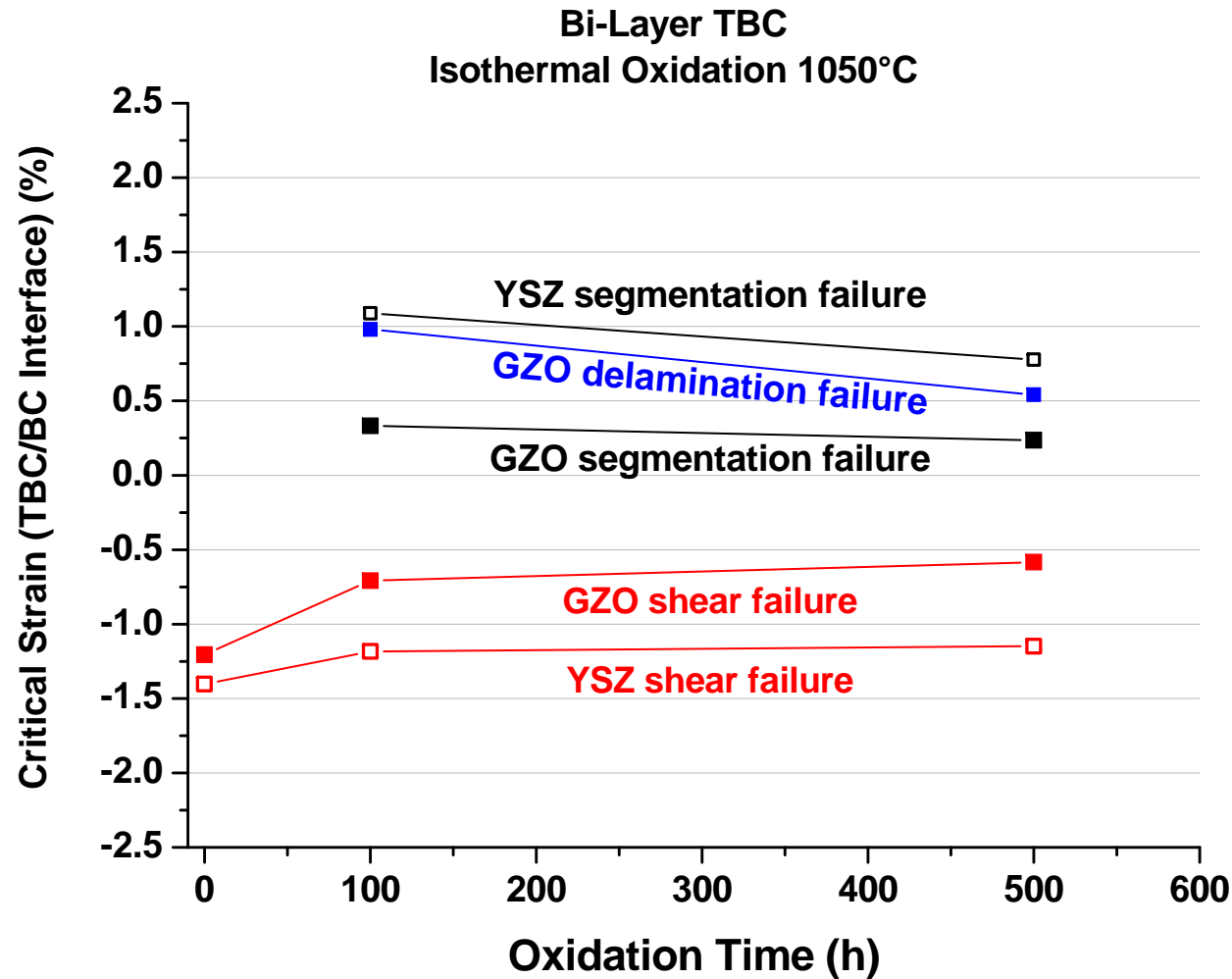


Macroscopic images do not provide sufficient insight. Only final failure can be observed.



1. Segmentation failure of GZO-layer
2. Delamination of GZO along GZO/YSZ interface
3. Segmentation failure of YSZ layer

Critical Strain Values



→ max. tolerable strain at TBC/BC interface

May be used in similar manner as SN-curves for lifetime assessment

Fracture Mechanics Approach

Griffith-Criterion:

$$\sigma_c = \frac{K_c}{\sqrt{\pi c}}$$

$$\varepsilon = \frac{\sigma}{E}$$

Critical Strain:

$$\varepsilon_c = \frac{K_{Ic}}{f \cdot E_{TBC} \sqrt{\pi c}}$$

Material Constant

(But: Measurements may be influenced by sample history)

Geometry Factor (Defect geometry)

Possible Values:

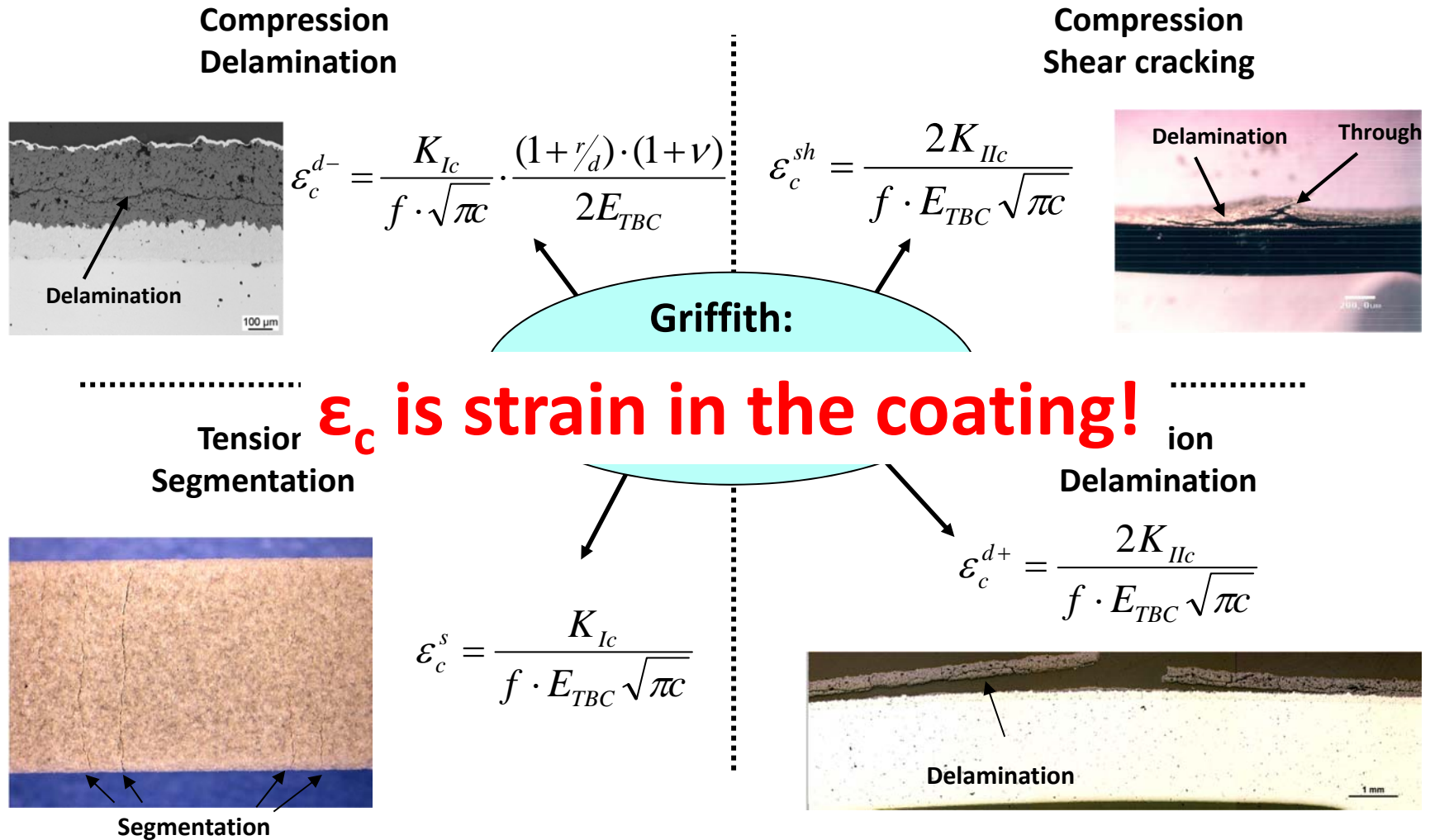
- 1.12 surface defect of infinite length
- 1.0 buried defect
- 0.64 semi-circular surface defect

Damage Parameters

c – defect size

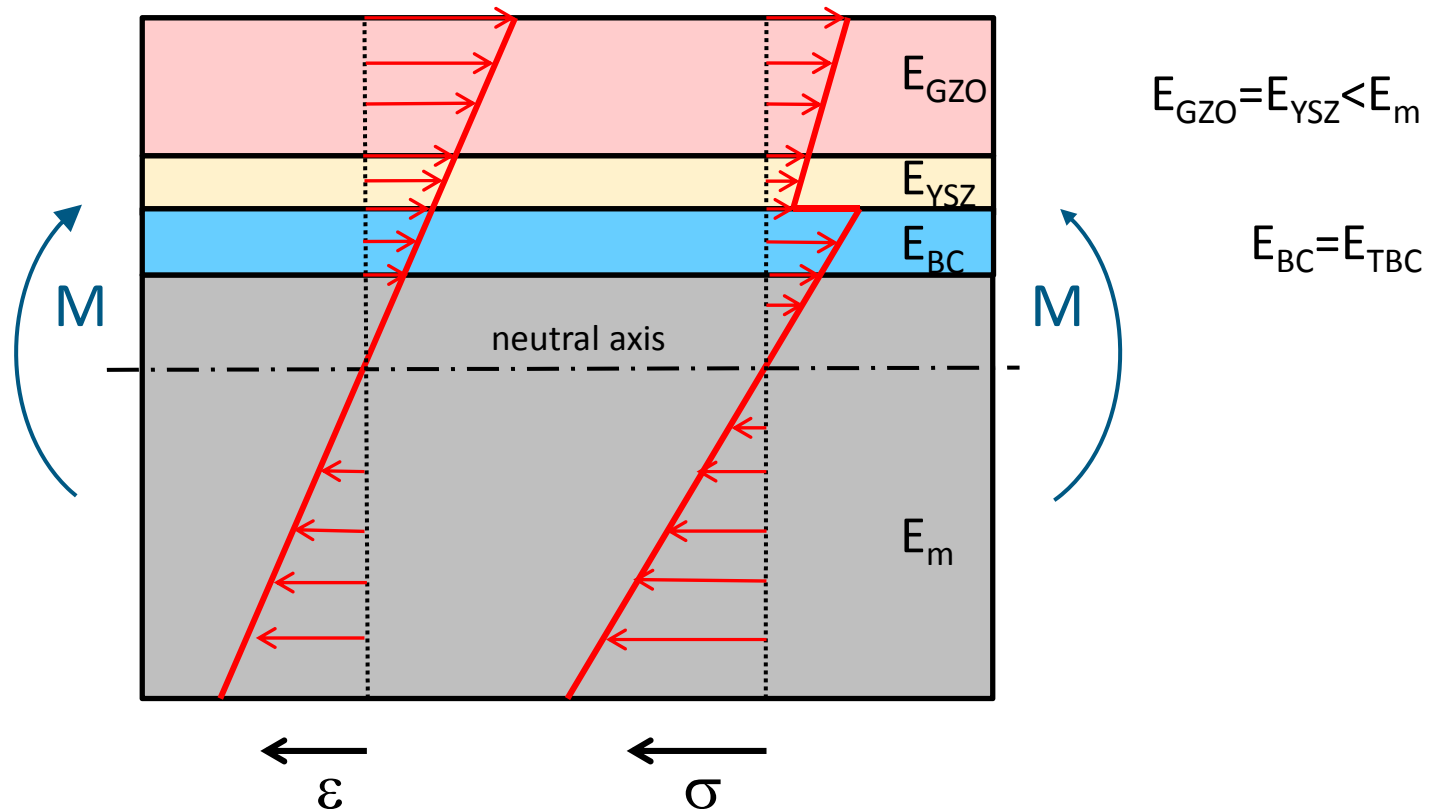
E – Young's modulus

Possible Failure Modes in 4-Point Bending



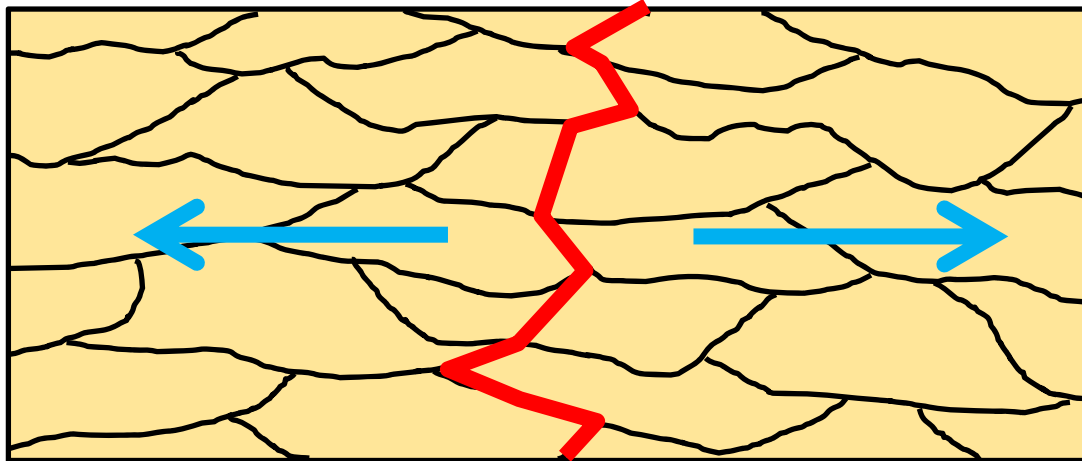
M. Schütze, Protective Oxide Scales and their Breakdown, John Wiley, (1997)

Strain gradient across the TBC-thickness under pure bending



~30% difference in strain between
TBC/BC interface and outer fiber for 500 μ m TBC
→ Failure position has to be considered!

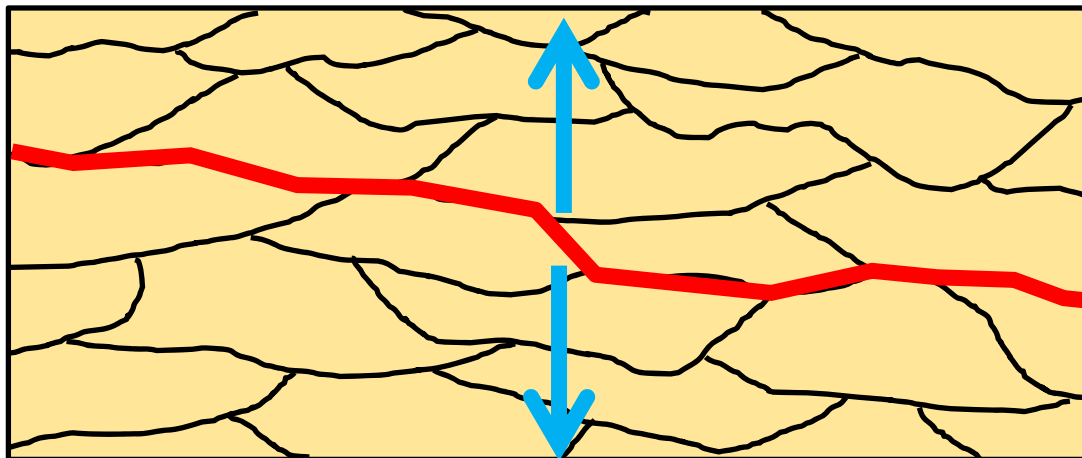
Microstructure has an influence on K_{Ic} -values



crack path mostly
through spray flats

$K_{Ic}(\text{path1})$

e.g. tensile segmentation



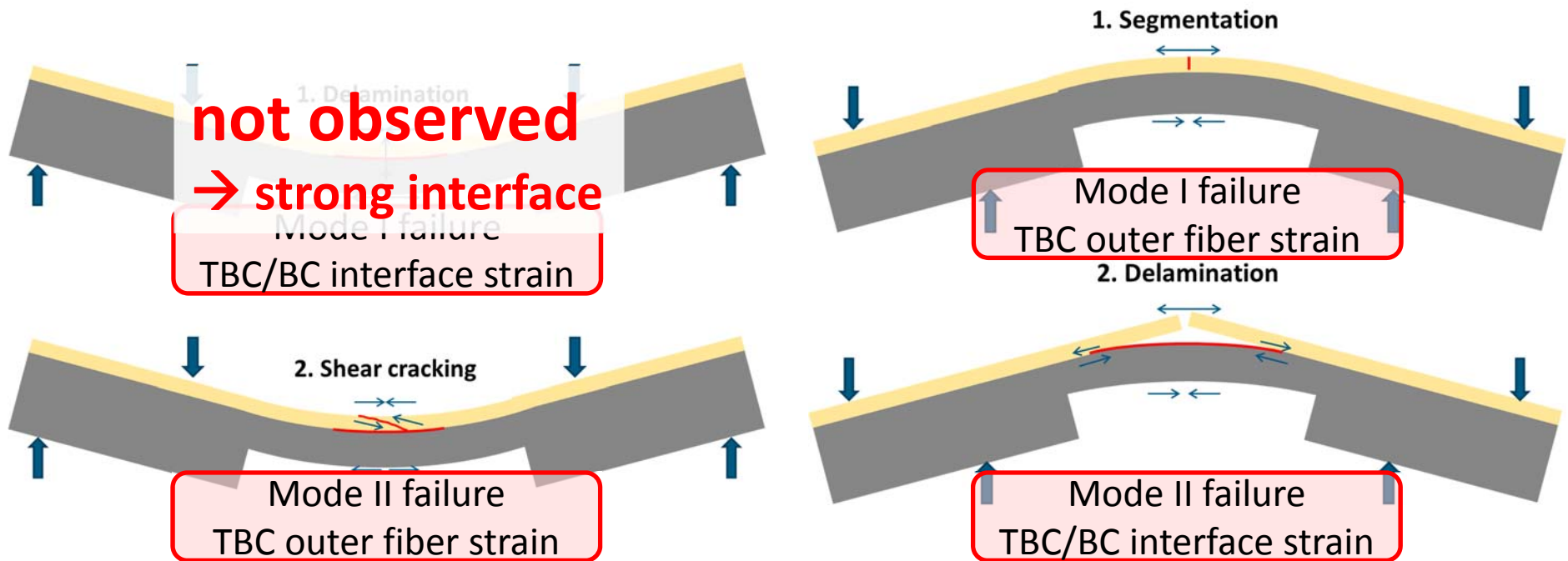
crack path along
spray flat boundaries

$K_{Ic}(\text{path2})$

e.g. compressive
delamination

$$K_{Ic}(\text{path1}) > K_{Ic}(\text{path2})$$

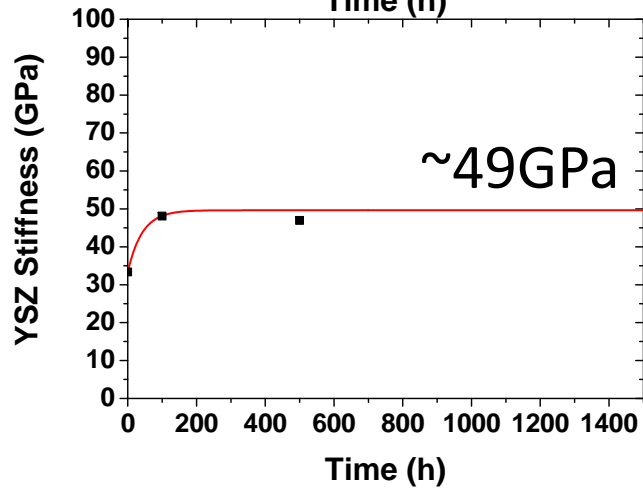
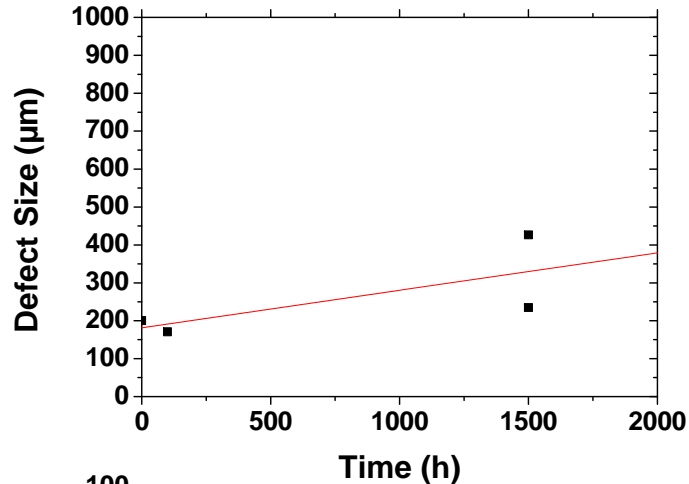
Chosing failure mode and critical strain position



Modeling input values

$$\varepsilon_c = \frac{K_c}{f \cdot E_{TBC} \sqrt{\pi c}}$$

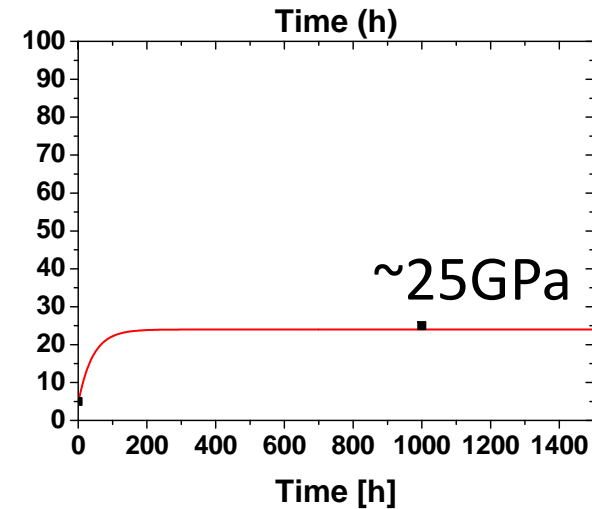
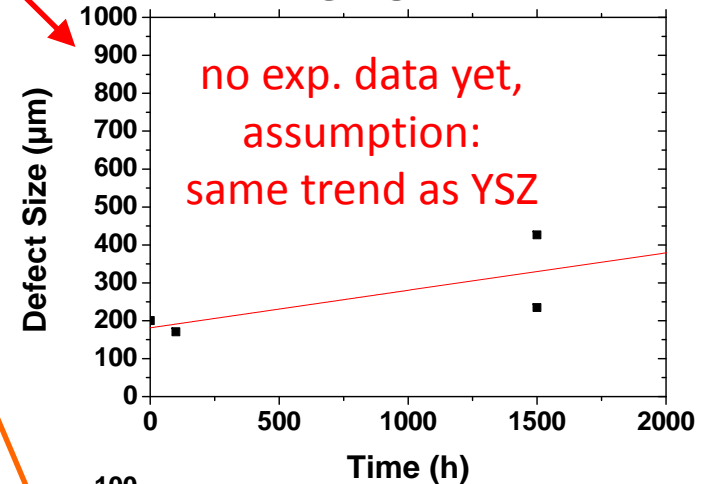
YSZ



$$K_{Ic} = 5.3 \text{ MPa m}^{1/2}$$

$$K_{IIc} = 10.6 \text{ MPa m}^{1/2}$$

GZO



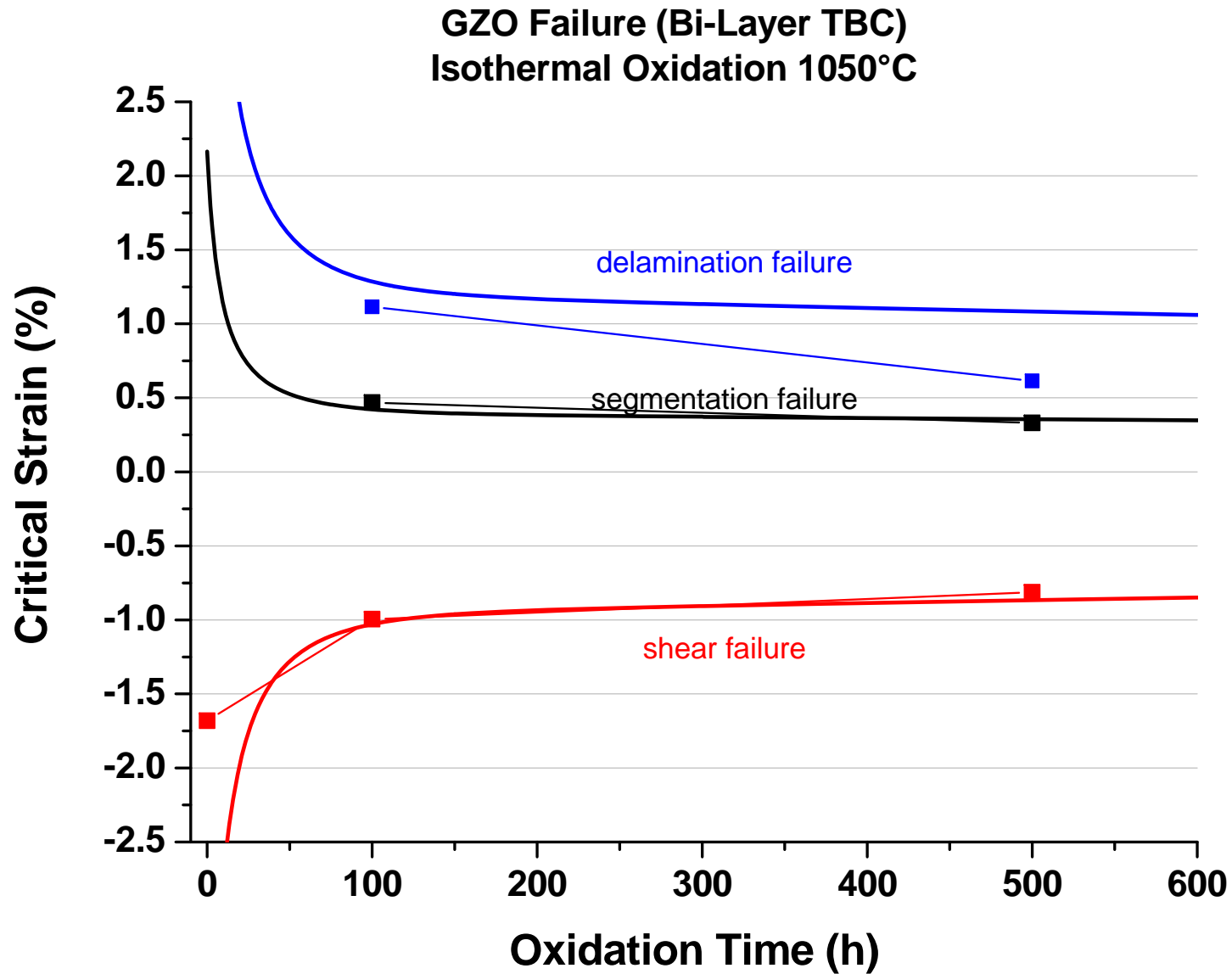
$$K_{Ic} = 2.3 \text{ MPa m}^{1/2}$$

$$K_{IIc} = 2.8 \text{ MPa m}^{1/2}$$

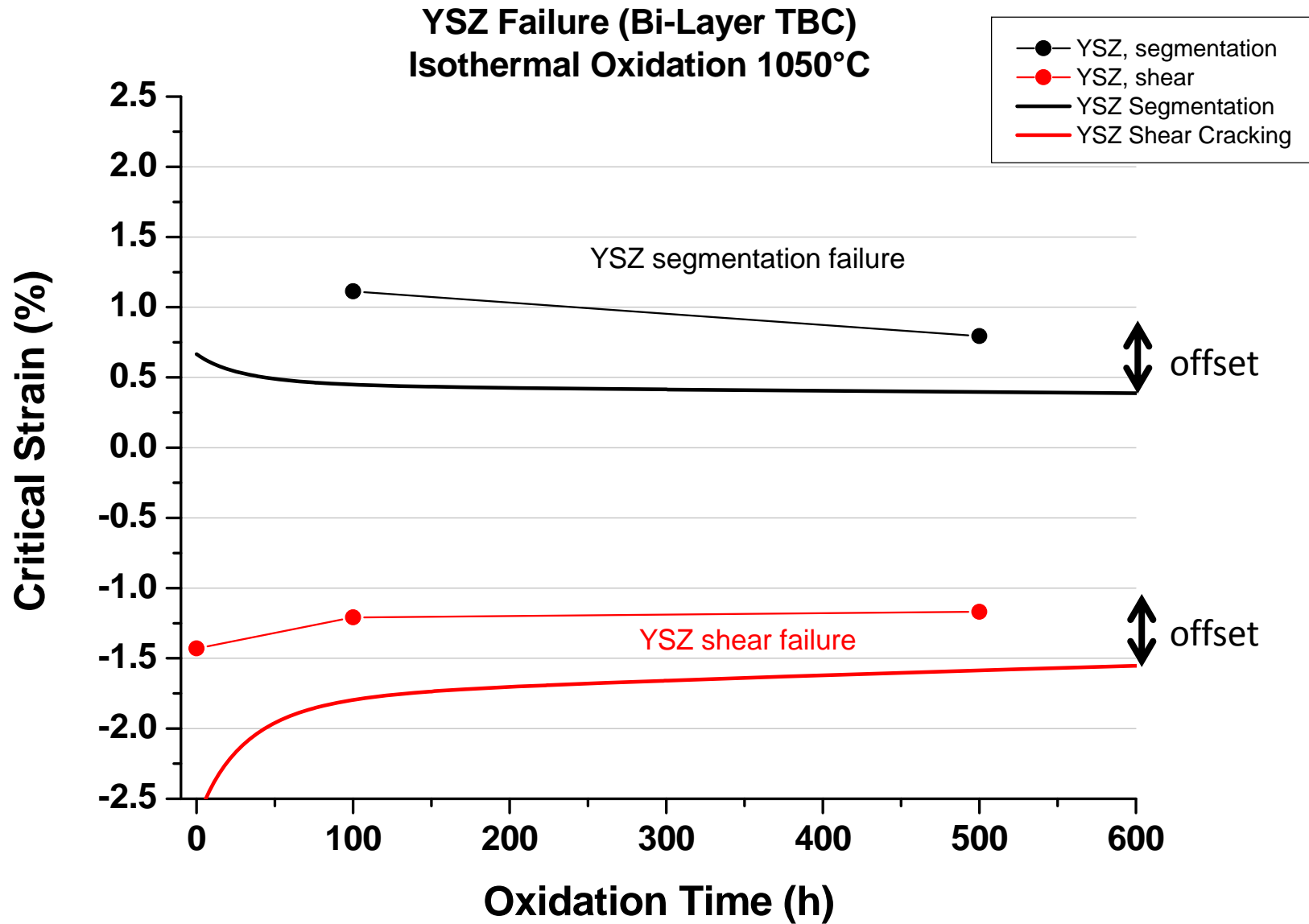
$f = 1.0$
(buried defect)

K_c currently used as fitting parameter!

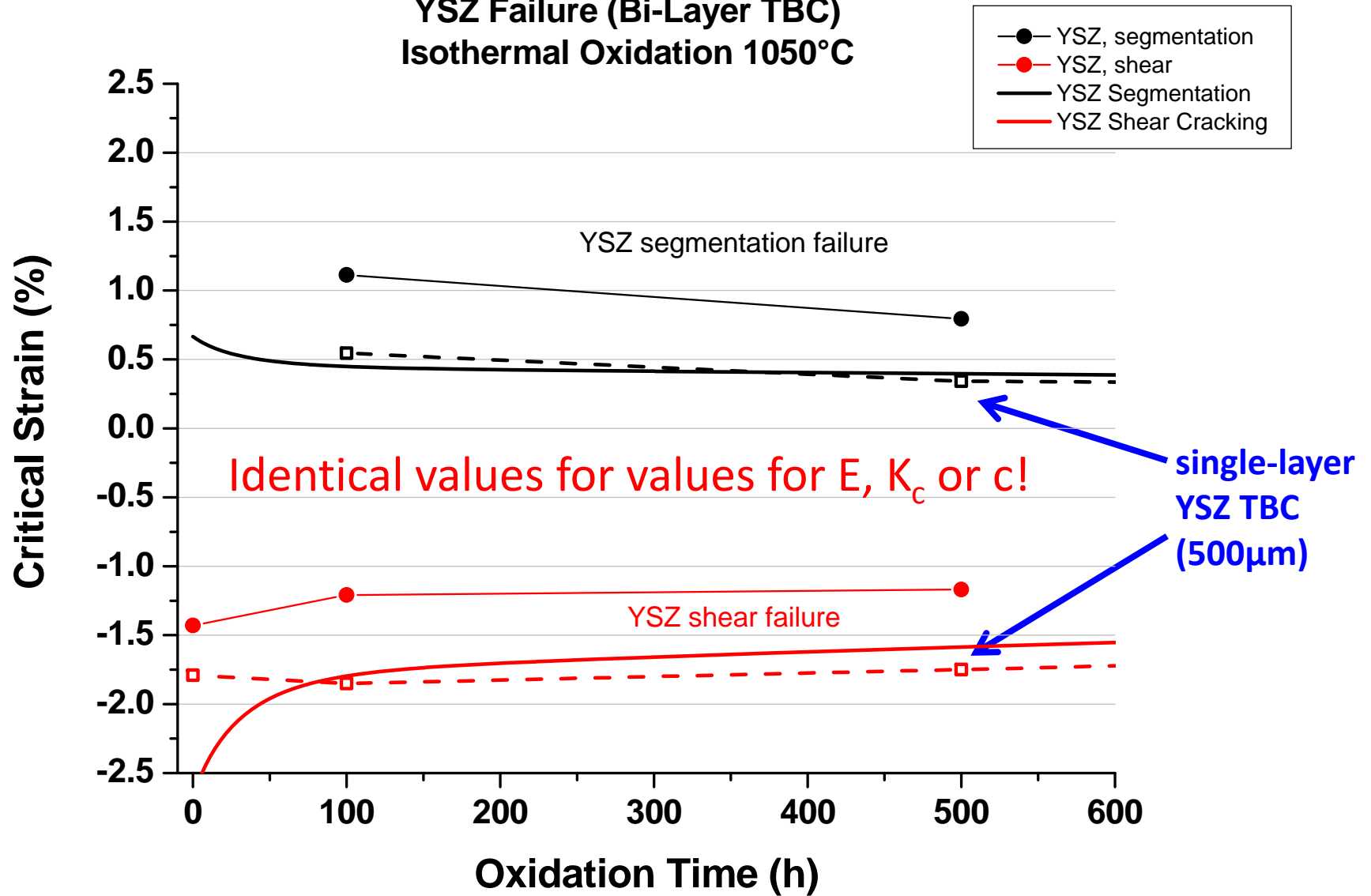
Bi-Layer System – GZO Failure



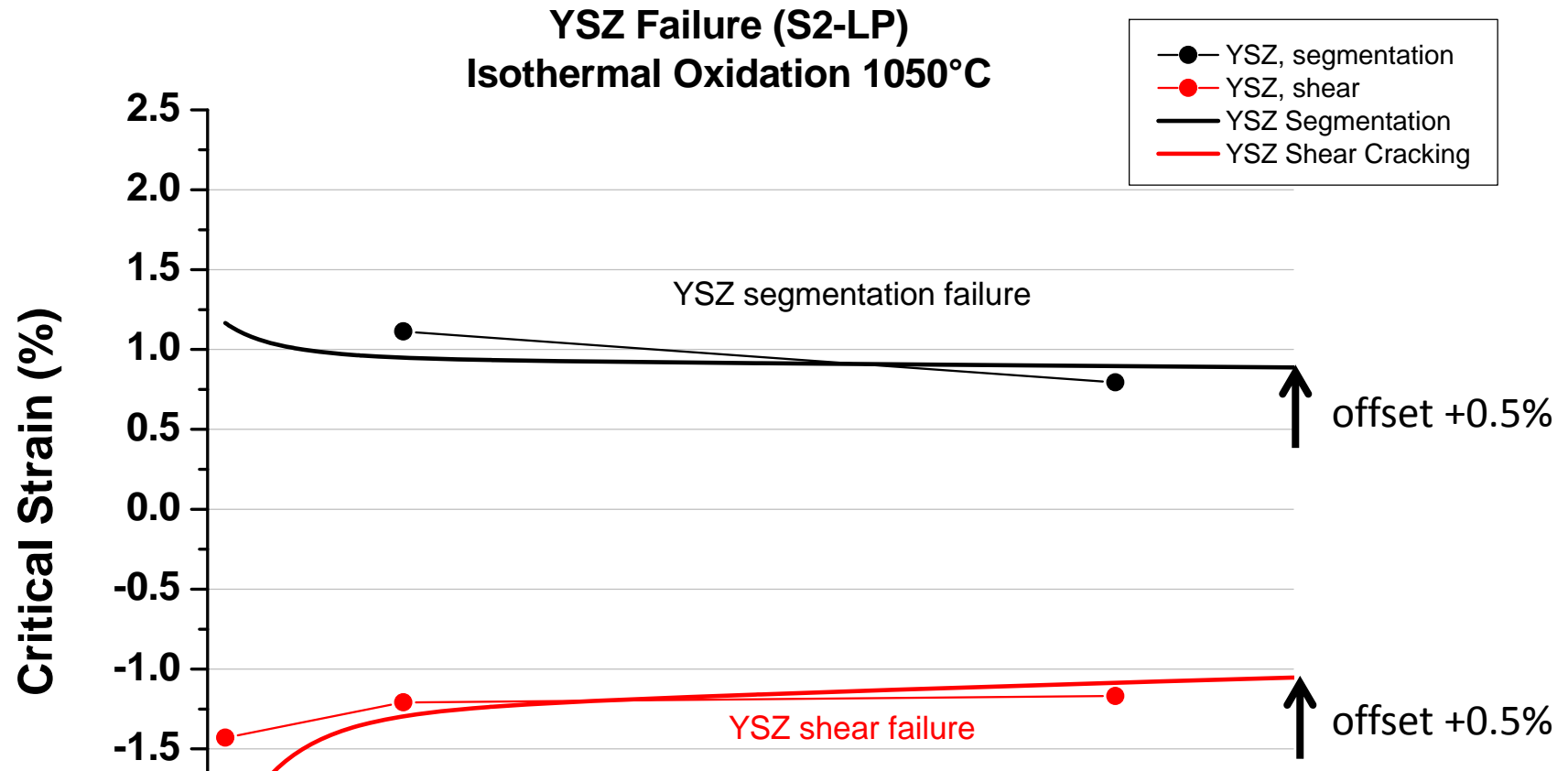
Bi-Layer System – YSZ Failure



YSZ Failure (Bi-Layer TBC) Isothermal Oxidation 1050°C



Bi-Layer System – YSZ Failure



Possible explanation for offset:

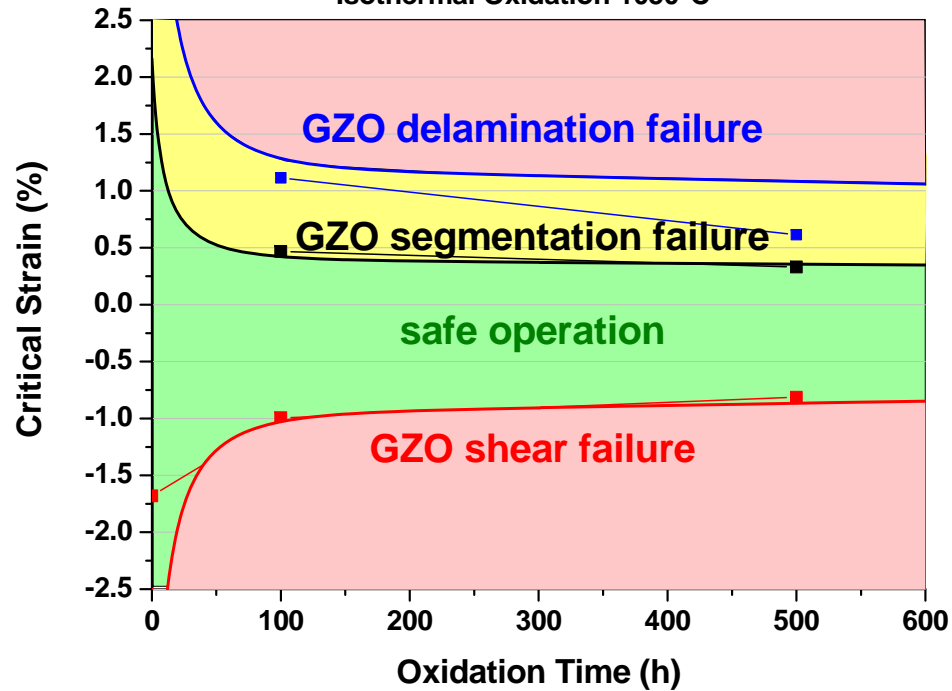
Residual stresses in the TBC are relieved by GZO failure prior to measurement of YSZ failure.

...currently under investigation!

Mechanical Stability Diagrams

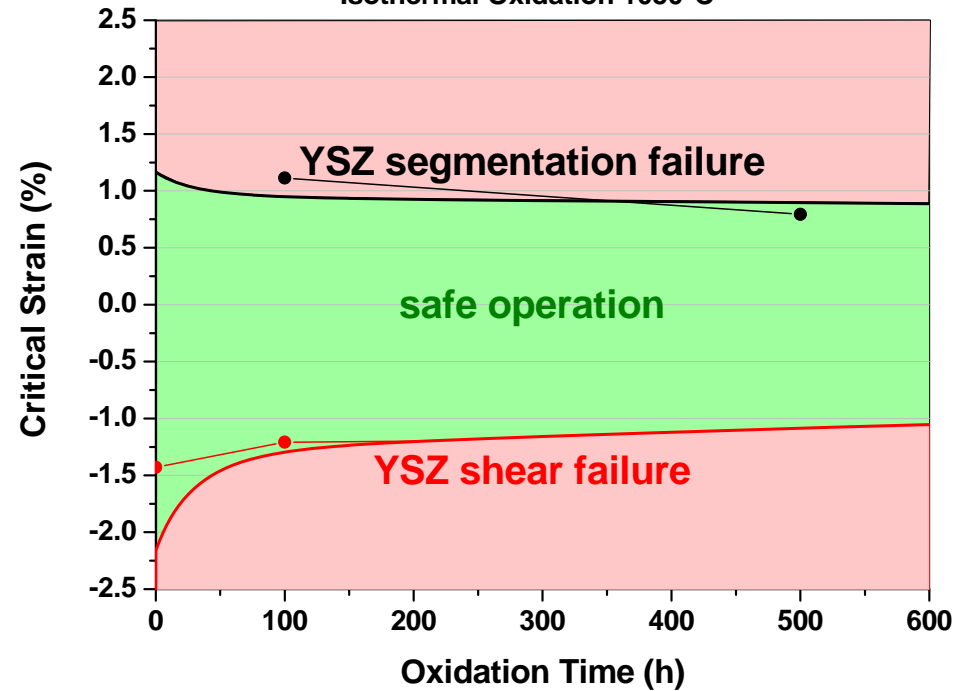
GZO Failure

Isothermal Oxidation 1050°C



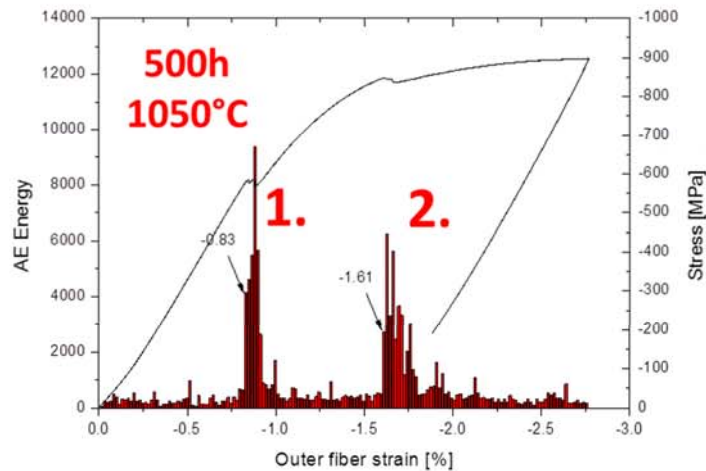
YSZ Failure

Isothermal Oxidation 1050°C



Summary

- Mechanical 4-point bending with in-situ acoustic emission measurement is a valuable tool to assess damage processes in bi-layer TBCs
- A modeling approach for bi-layer TBCs has been developed to delineate areas of safe operation from areas where failure is imminent -> mechanical stability diagram



Thank you for your attention!

