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Kinetic enhancement of adsorbent for CO₂ capture from atmosphere by porous material

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CO₂ Summit II:
Technologies and Opportunities

Kinetics Enhancement of Adsorbents for CO₂ Capture from Atmosphere by porous Materials

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Outline

1 Background

2 Experiments and model

3 Results and discussion

4 Conclusion

R&D — Capture Material

Wild absorbent

Na- or Ca-based sorbents with high heats of adsorption and high regeneration temperatures, e.g. 800 to 1200 K

Mild absorbent

Amine-functionalized porous solids, slow kinetics

Institute	Absorbent	Reaction atmosphere	Capacity mmol/g	Application
Georgia Tech.	PEI/silica	air	2.36	CO ₂ air capture
Columbia Uni.	Ion exchange resin	air	1.73	CO ₂ air capture
Hamburg Uni. of Tech.	Amino - silica	2500ppm	1.55	CO ₂ removal submarines, space crafts or aircraft
<i>United Tech. Res. Center</i>	HSC+	2%	1.82	CO ₂ removal in space shuttle applications
Korea Uni.	MOFs	Air	2.82	CO ₂ air capture

R&D — Capture Material

Research on CO₂ removal under ultra-dilute atmosphere in China

Institute	Absorbent	Reaction atmosphere	Capacity	Application
Zhejiang university	CNTs/TEPA、TETA	2% CO ₂	2.52-3.56 mmol/g	CO ₂ removal in confined space
PLA University of Science and Technology	LiOH	1% CO ₂	1.89 mmol/g	CO ₂ removal in submarine .etc
Tianjin university	5A molecular sieve	0.3%		CO ₂ removal in spacecraft
Zhejiang university	Ion-exchange resin	air	1.72 mmol/g	Air capture
The 718 research institute of CSIC	Hollow fiber membrane contactor	0.1%-0.5% CO ₂		CO ₂ removal in confined space

R&D — Air Capture Kinetics

- Could be much lower compared to flue gas capture due to the lower CO₂ partial pressure;

Inlet Concentration: 12 kPa : 40 Pa = 300:1

Efficiency: ↓90% ↓1%

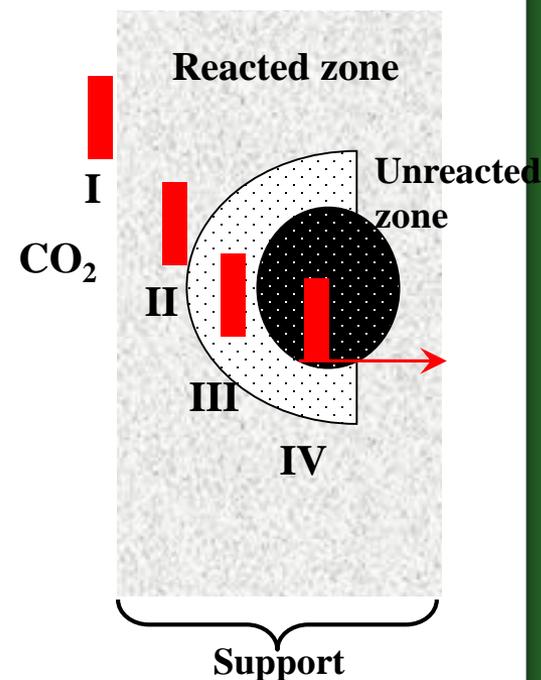
Outlet Concentration : 1.2 kPa : 40 Pa = 30:1

Adsorption kinetics is crucial to **reactor design** and the **optimization of adsorption material**, but reports related are limited.

R&D — Air Capture Kinetics

The kinetics is expected to be improved by immobilizing functional group onto solid supports with large surface area, such as mesoporous silica, alumina and carbon black.

Material	Pore size (nm)	Surface area m^2/g (Before)	Surface area m^2/g (After)	Adsorption half time, (mins)
FS-PEI	1.057	--	79.9	300
T-PEI/silica	--	--	--	210
HAS6	5-6	200-500	71	100-150
AEAPDMS-NFC-FD	--	26.8	7.1	100
MOFS	--	3270	70	30
RFAS	7	--	150-300	10-20
Carbon Black	--	223	21	10



I: Boundary diffusion, II: Support diffusion
 III: Product diffusion, IV: Reaction

However, the inappropriate material selection or treatment process for sorbent could result in unexpected diffusion resistance.

Methodology of Kinetics Analysis

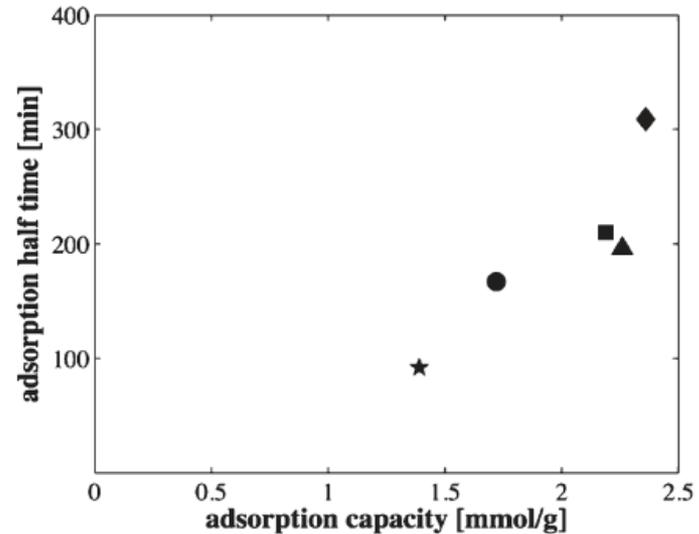
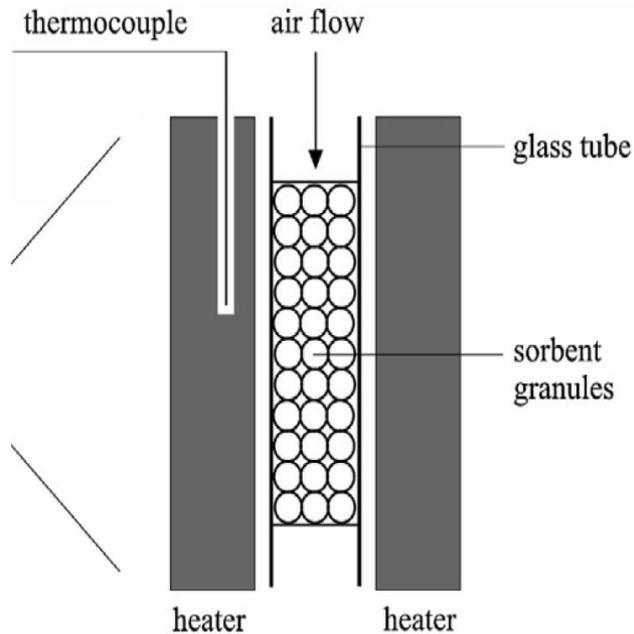


Figure 5. Comparison of adsorption capacity and adsorption half time of AEAPDMS-NFC-FD (star), HAS6 (sphere), PEI/silica (rhombus), A-PEI/silica (triangle), T-PEI/silica (square).^{6,7}

Int. J. Greenhouse Gas Control, 2013, 17, 332-340

Environ. Sci. Technol. 2011, 45, 9101-9108

Experiment- The resistance from gas side diffusion is hard to be avoided on the fixed bed reactor.

Model- The existing indicator of half time is too simple to reflect the real reaction process under ultra low CO₂ concentration.

Outline

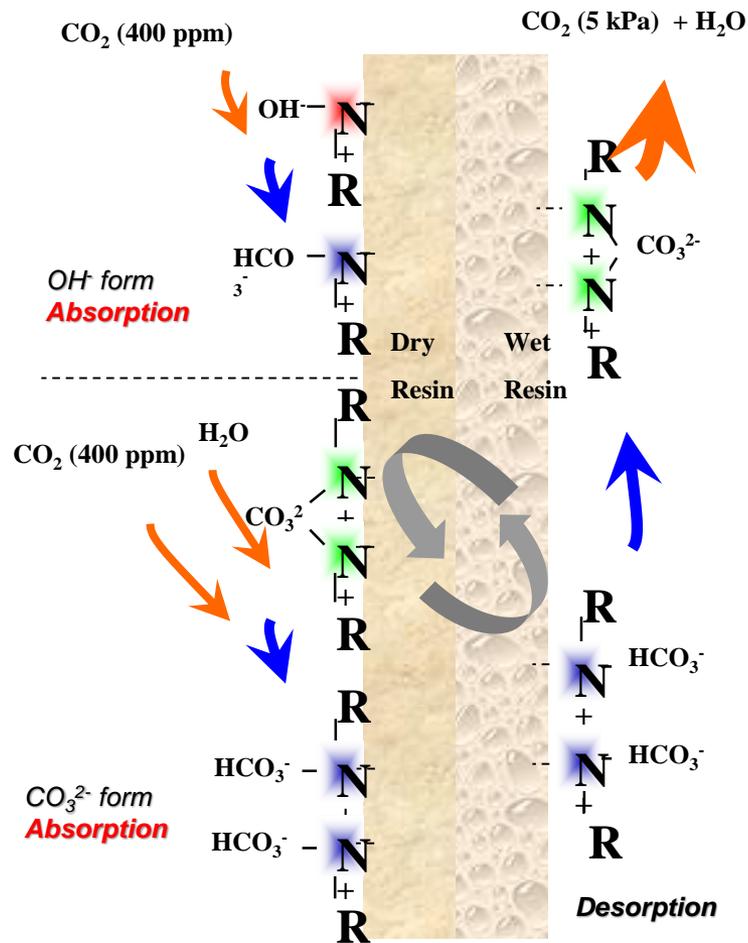
1 Background and motivation

2 Experiments and model

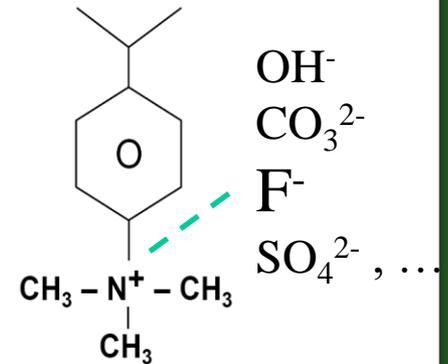
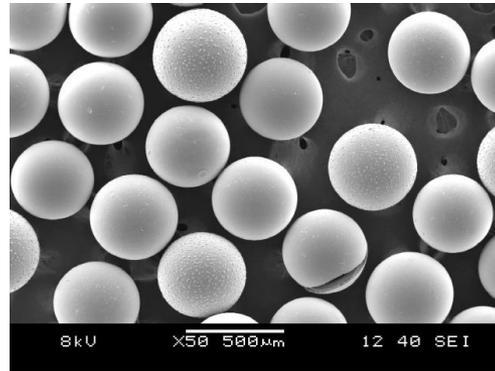
3 Results and discussion

4 Conclusion

Experimental material



Ion Exchanged Resin Material



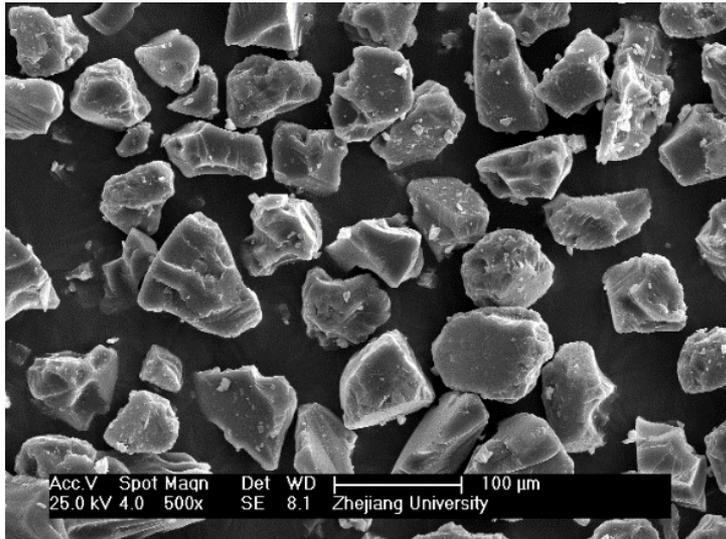
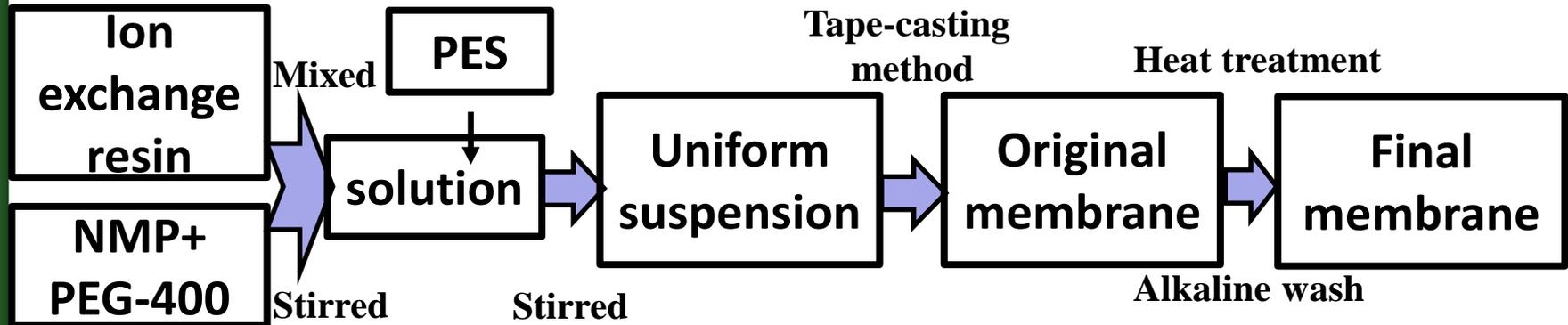
Developed and tested by Columbia University

Eur. Phys. J., 2009, 176, 93-106;

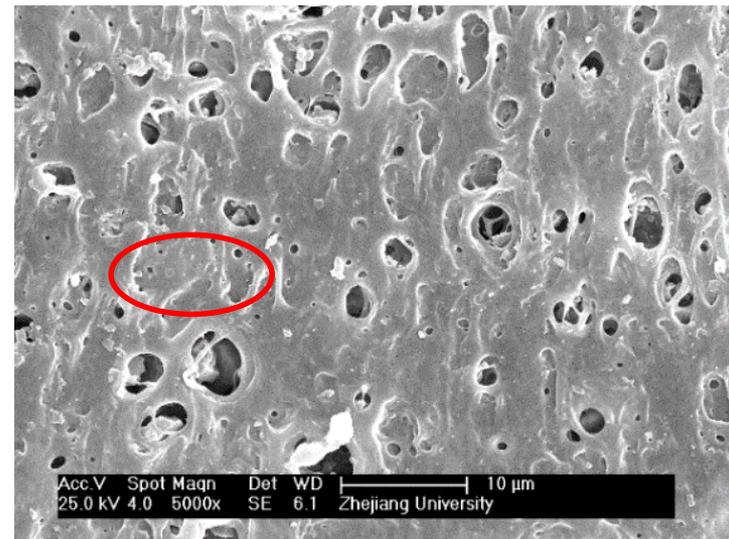
Environ. Sci. Technol., 2011, 45, 6670-6675.

An economically viable air capture method by avoiding expensive heating/cooling cycles or significant pressure changes.

Preparation of adsorption material

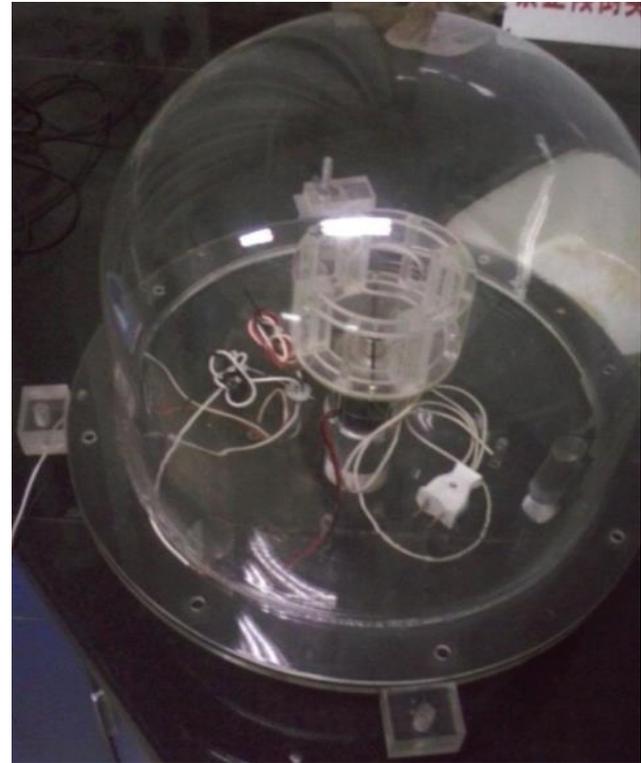
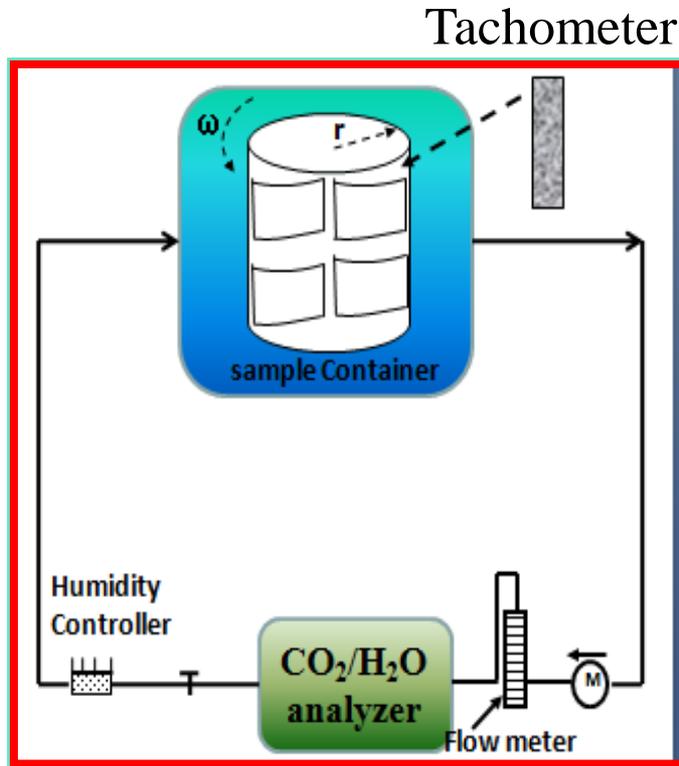


Resin with uniform size



Membrane with Porous structure

Experimental system



Experiment- *A revolving bed reactor is built to characterize the mass transfer limitations of CO₂ adsorption with relatively low kinetics.*

Kinetics model

Model-the shrinking core model is modified to analyze the resistance during CO_2 absorption

Support layer diffusion

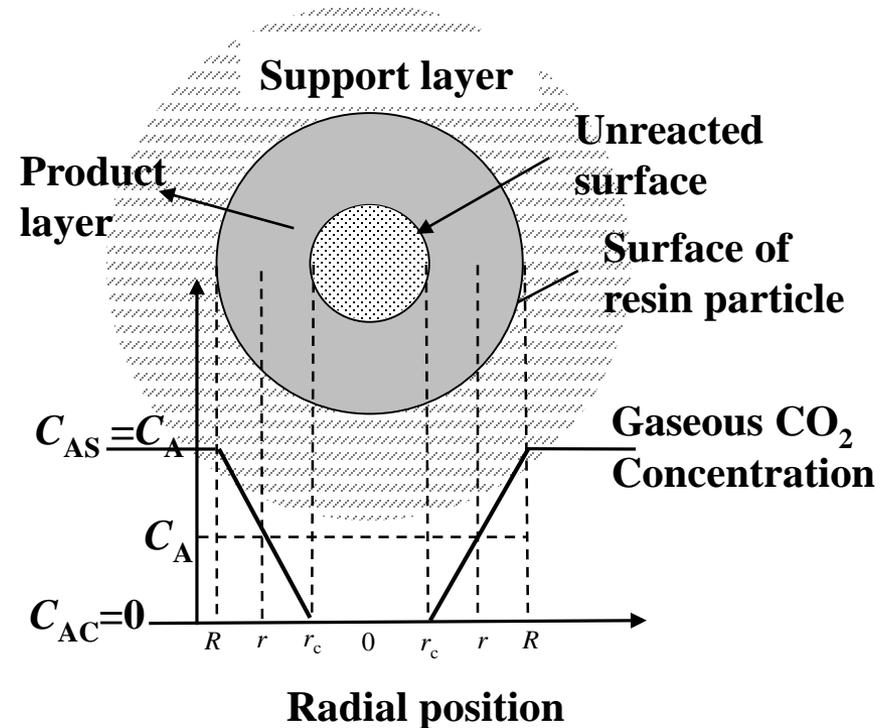
Fick' Law:

$$-\frac{dN'_{CO_2}(t)}{dt} = SQ_A = SD_{e1} \frac{2(C_1 - C_2)}{L}$$



Support layer diffusion rate:

$$V_{\text{film}} = D_{e1} \frac{C_0}{2\rho L^2}$$



Kinetics model

Product layer diffusion rate :

$$V_{\text{diff}} = \frac{3D_{e2}C_0}{R^2 \rho_2 [(1 - \theta / \theta_{\text{max}})^{-1/3} - 1]}$$

*The unknown parameter:
product layer diffusion coefficient*

Chemical reaction rate:

$$V_{\text{diff}} = \frac{3kC_0(1 - \theta / \theta_{\text{max}})^{2/3}}{\rho_2 R}$$

*The unknown parameter:
Chemical reaction rate coefficient*

The total resistance during CO2 adsorption:

$$\lambda = \frac{L^2 \rho_1}{2D_{e1}C_0} + \frac{\rho_2 R^2 [(1 - \theta / \theta_{\text{max}})^{-1/3} - 1]}{3D_{e2}C_0} + \frac{\rho_2 R}{3kC_0(1 - \theta / \theta_{\text{max}})^{2/3}}$$

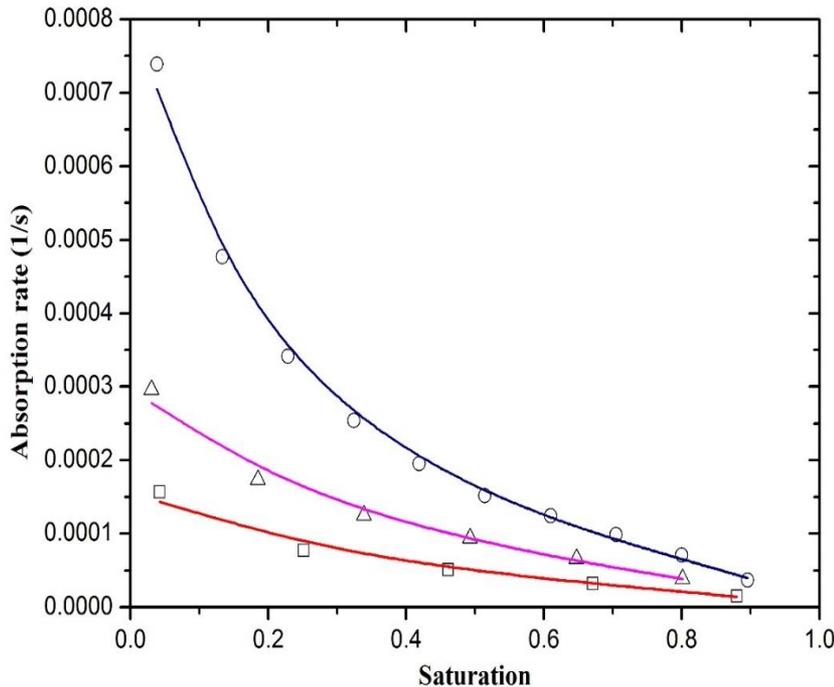
1 Background

2 Experiments and model

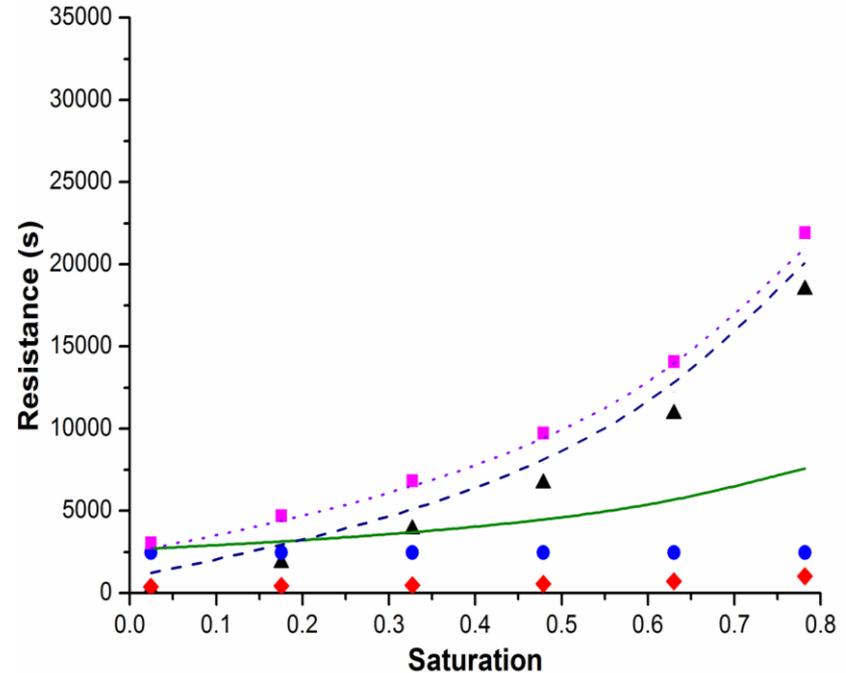
3 **Results and discussion**

4 Conclusion

The effect of particle size

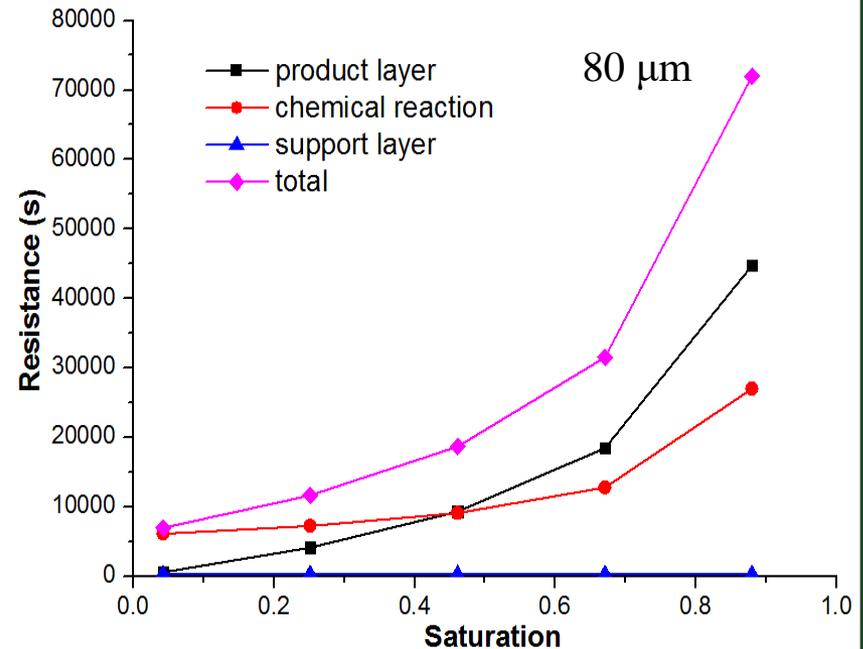
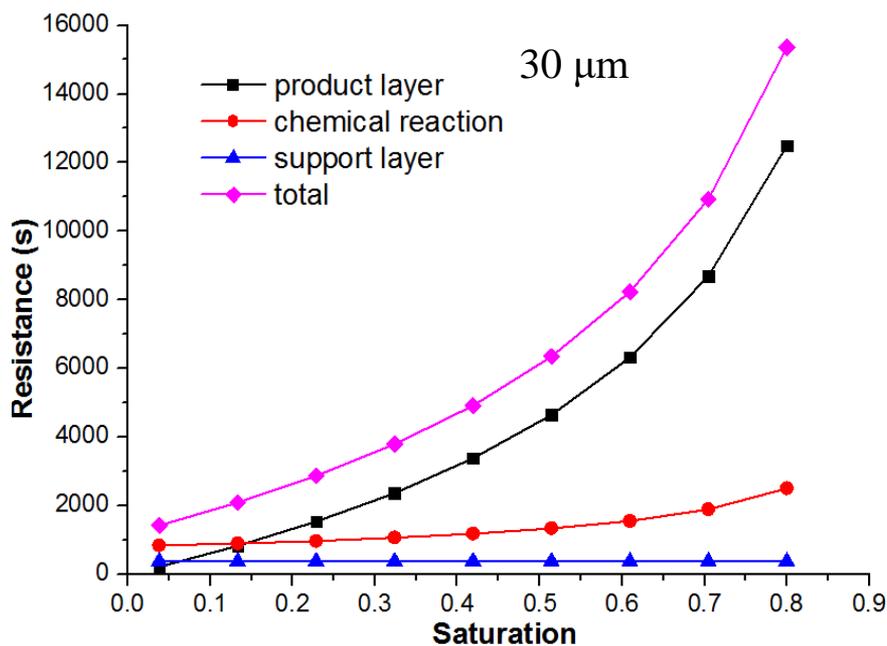


Kinetics at different sorbent size (dots are experimental data, square: diameter of 80 μm; triangle: diameter of 40 μm; circle: diameter of 30 μm; solid lines are the fitting date)



Resistance contributions from different steps at 0.5% vapor concentration. (square: total resistance; diamond: reaction resistance; triangle: production resistance; circle: support resistance; dashed line: total resistance (L/2); solid line: total resistance (R/2); dot line: total resistance (10k))

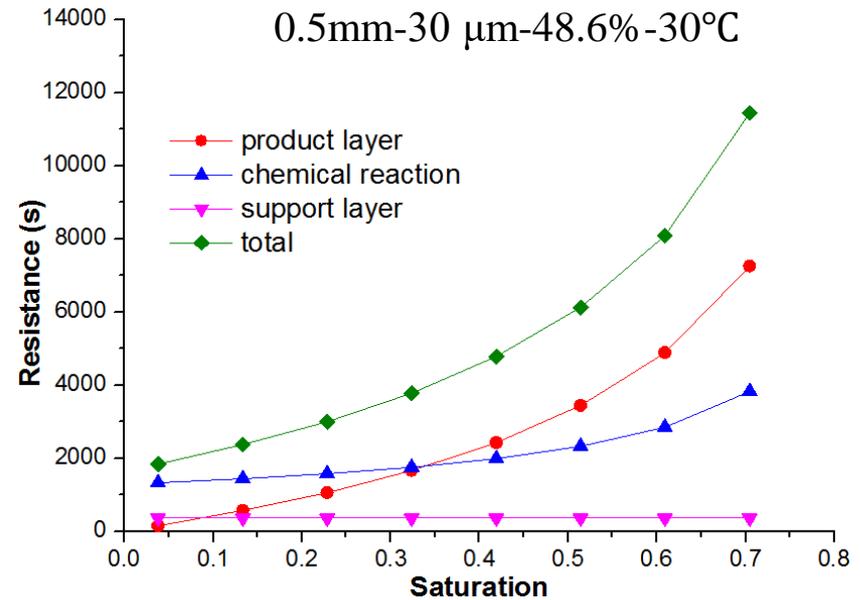
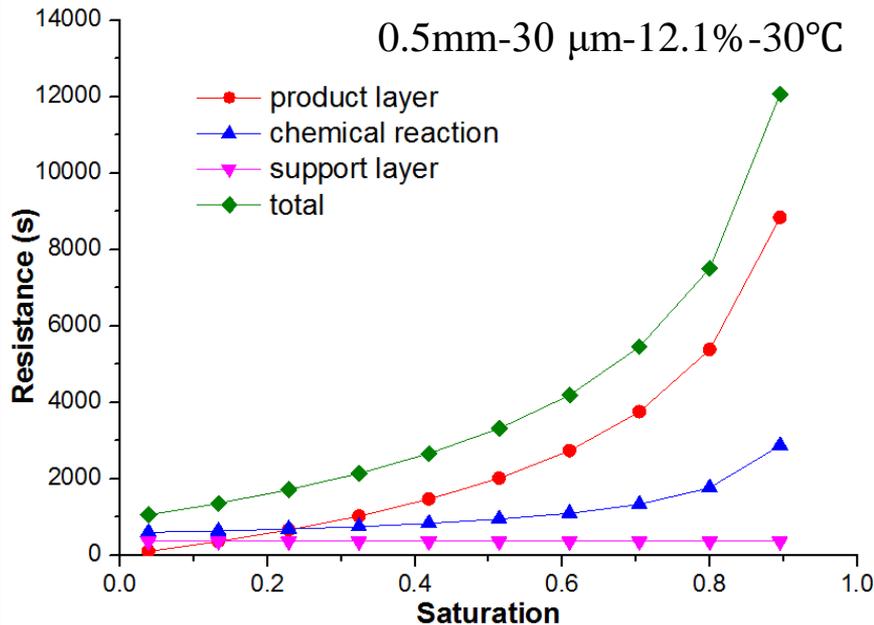
The effect of particle size



Decomposition of mass transfer resistance under different particle size. (20 °C and 21.2% relative humidity)

The adsorption rate increases significantly with decreasing sorbent size, indicating a resin particle dominated kinetics, rather than support layer dominated kinetics.

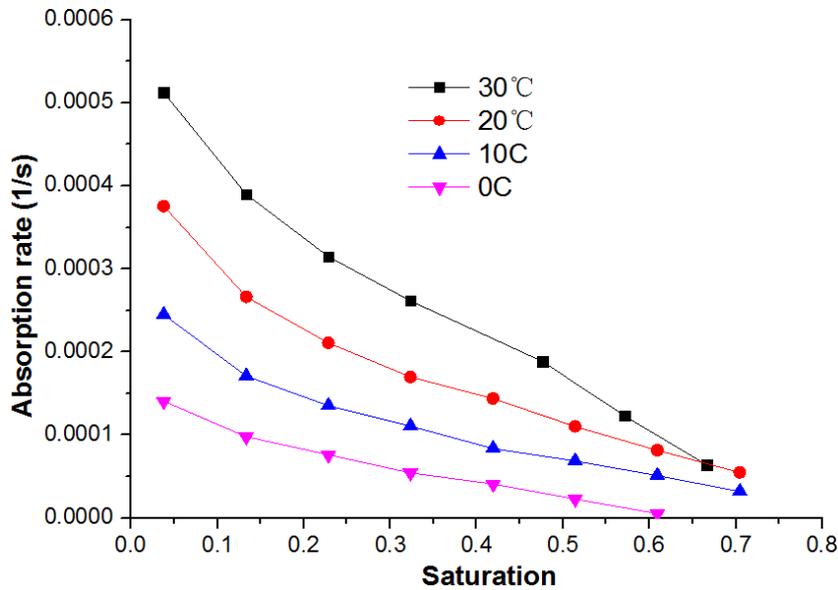
The effect of humidity



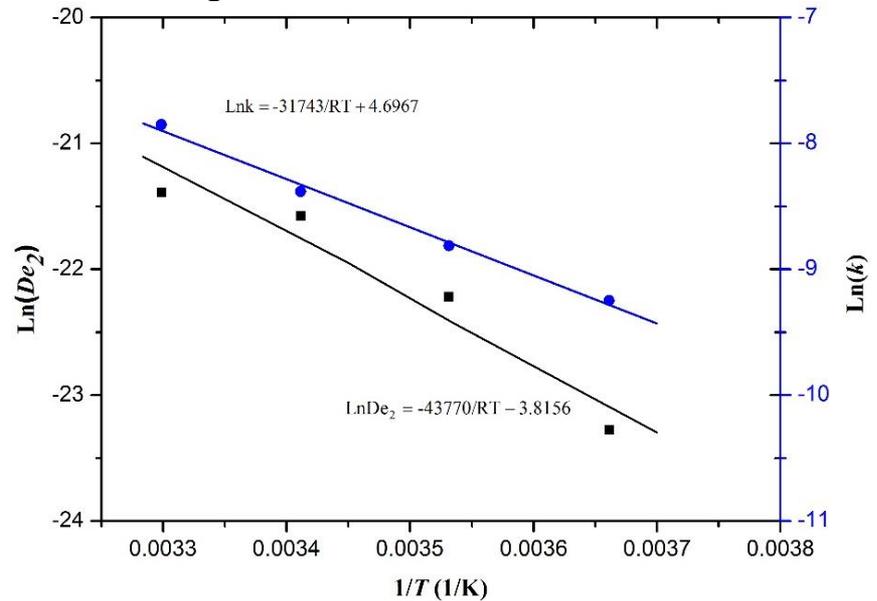
Decomposition of mass transfer resistance under different humidity.

The relative humidity affects the rates of physical diffusion and chemical reaction simultaneously, and it impacts the chemical reaction more significantly than physical diffusion in the moisture swing adsorption.

The effect of temperature



Absorption rate under different temperature.
(particle size: 30 μ m, 50% relative humidity)

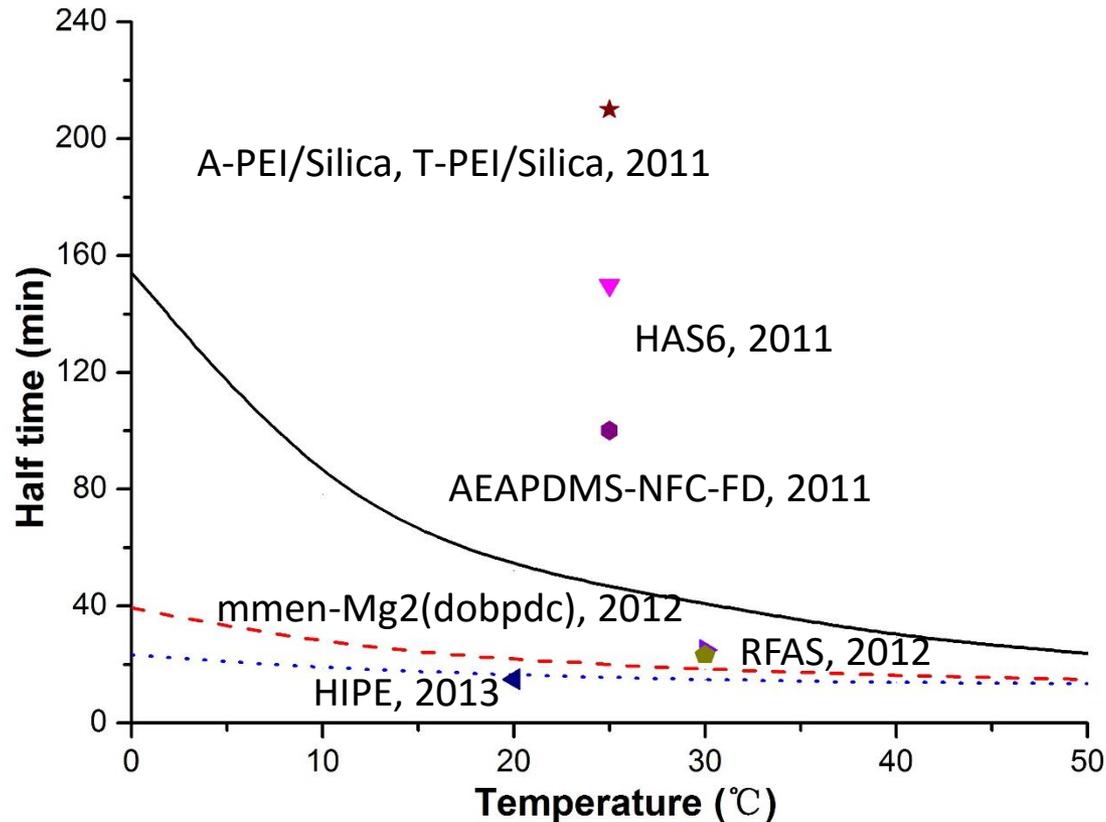


Temperature dependence of chemical reaction rate, k (m/s) and effective product layer diffusion coefficient, D_{e2} (m²/s).

$$\omega_i = A_i \exp(-E_{a-i} / (R_c T))$$

Where ω_i is the rate constant, A_i is the frequency factor, E_{a-i} is the activation energy, and R_c is the universal gas constant. The A_i and E_{a-i} can be determined by linear fitting as shown in Fig. The activation energy of chemical reaction is 31.7 kJ/mol, which is at the same level as reported for amine based reaction with CO₂

$$t = \int \left(\frac{2\rho_1 L^2}{D_{e1} C_0} + \frac{R^2 \rho_2 [(1 - \theta / \theta_{\max})^{-1/3} - 1]}{3D_{e2} C_0} + \frac{\rho_2 R}{3kC_0 (1 - \theta / \theta_{\max})^{2/3}} \right) d\theta$$



Comparison of CO₂ adsorption half time with different adsorbents. Solid line: 30 μm, dash line: 10 μm, dot line: 5 μm. Scattered dots are experimental data in literatures.

Conclusion

- the adsorption kinetics could be enhanced by employing sorbent with smaller particles
- Both the diffusion coefficient and chemical reaction constant drop significantly with decreasing temperature or increasing relative humidity.
- The sorbent exhibits significant product layer diffusion controlled kinetics
- By preparing sorbent with μm sized particles, the half-time of sorbent in this study could reach the same level of recently developed air capture sorbent with much more expensive material, such as MOFs and nanomaterial.